





Validation of the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 Cross Section Libraries on the PCA-Replica (Water/Iron) Neutron Shielding Benchmark Experiment

Massimo Pescarini, Roberto Osi, Manuela Frisoni

Report RdS/PAR2013/077

Validation of the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 Cross Section Libraries on the PCA-Replica (Water/Iron) Neutron Shielding Benchmark Experiment

Massimo Pescarini, Roberto Orsi, Manuela Frisoni - ENEA

Settembre 2014

Report Ricerca di Sistema Elettrico

Accordo di Programma Ministero dello Sviluppo Economico - ENEA Piano Annuale di Realizzazione 2013 Area: Produzione di energia elettrica e protezione dell'ambiente Progetto: Sviluppo competenze scientifiche nel campo della sicurezza nucleare e collaborazione ai programmi internazionali per il nucleare di IV Generazione Obiettivo: Sviluppo competenze scientifiche nel campo della sicurezza nucleare Responsabile del Progetto: Felice De Rosa, ENEA



Distrib.	Pag.	
n L 🚣	1	11

Titolo

Validation of the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 Cross Section Libraries on the PCA-Replica (Water/Iron) Neutron Shielding Benchmark Experiment

Descrittori

Tipologia del documento:	Rapporto tecnico
Collocazione contrattuale:	Accordo di programma ENEA-MSE su sicurezza nucleare e
	reattori di IV generazione
Argomenti trattati:	Fisica nucleare, dati nucleari, fisica dei reattori nucleari

Sommario

Three-dimensional (3D) fixed source transport calculations in Cartesian (X,Y,Z) geometry for the PCA-Replica 12/13 water/iron (H₂O/Fe) engineering neutron shielding benchmark experiment were performed with the TORT-3.2 discrete ordinates (S_N) code. The ENEA-Bologna BUGJEFF311.BOLIB (JEFF-3.1.1 data) and BUGENDF70.BOLIB (ENDF/B-VII.0 data) broad-group coupled (47 n + 20 γ) working cross section libraries in FIDO-ANISN format together with the similar ORNL BUGLE-96 (ENDF/B-VI.3 data) library, specifically conceived for LWR shielding and pressure vessel dosimetry applications, were alternatively used together with dosimeter cross sections, processed from the IAEA IRDF-2002 dosimetry file. The ENEA-Bologna programs ADEFTA-4.1 and BOT3P-5.3 were respectively employed for the calculation of the isotopic atomic densities and for the automatic generation of the spatial mesh grid of the geometrical model. The calculated integral and spectral results were compared with the corresponding experimental data, respectively obtained with threshold activation dosimeters (Rh-103(n,n')Rh-103m, In-115(n,n')In-115m and S-32(n,p)P-32), spherical hydrogen-filled proportional counters (type SP-2) and a spherical organic liquid (NE213) scintillator. PCA-Replica, reproducing the ex-core geometry of a PWR, is particularly fit to test the cited working libraries since it was specifically conceived to check calculated fast neutron fluxes in a PWR mild steel pressure vessel simulator.

Note

Authors: Massimo PESCARINI, Roberto ORSI, Manuela FRISONI

Сор	ia n.		In carico a	a:		
2	л эллэ, цэг 1, g	Part and and I	NOME	interen Spectra Cap. Inter BUGIBPENN	an kat U	9371128
			FIRMA			
1	a and a	COLUMN 24	NOME	ins BUGENDF70	a Alo aU	
			FIRMA			TIT POIL O
0	EMISSIONE	14/07/2014	NOME	M. Pescarinj	F. Padoani	F/ De Rosa
EIMISSIONE	14/07/2014	FIRMA	M. Rescer in	Herolloe.	Lefrer/hilme	
REV.	DESCRIZIONE	DATA		REDAZIONE	CONVALIDA	APPROVAZIONE

di 118



INDEX

1 - INTRODUCTIO	ON	p. 3
2 - PCA-REPLICA	EXPERIMENT	p. 4
2.1 - PCA-Replie	ca Experimental Facility	p. 4
2.2 - PCA-Replie	ca Fission Plate	p. 10
2.3 - PCA-Replie	ca Experimental Measures	p. 15
3 - CROSS SECTIO	ON LIBRARIES AND NUCLEAR DATA	p. 18
3.1 - BUGJEFF3	311.BOLIB Cross Section Library	p. 18
3.2 - BUGENDF	70.BOLIB Cross Section Library	p. 18
3.3 - BUGLE-96	Cross Section Library	p. 19
3.4 - IRDF-2002	Dosimeter Cross Sections	p. 22
3.5 - U-235 Fissi	ion Neutron Spectra	p. 30
4 - TRANSPORT C	CALCULATIONS	p. 34
4.1 - Transport C	Calculation General Features	p. 34
4.2 - PCA-Replie	ca Fission Neutron Source	p. 43
4.2.1 - Inhom	ogeneous Neutron Source	p. 43
4.2.2 - Homog	geneous Neutron Source	p. 43
5 - DISCUSSION O	OF THE RESULTS	p. 45
5.1 - Dosimetric	Results	p. 45
5.2 - Spectral Re	esults	p. 68
6 - CONCLUSION		p. 79
REFERENCES		p. 80
APPENDIX A	Neutron Spectra Calculated along the Horizontal Axis Z Using BUGJEFF311.BOLIB	p. 83
APPENDIX B	Neutron Spectra Calculated along the Horizontal Axis Z Using BUGENDF70.BOLIB	p. 95
APPENDIX C	Neutron Spectra Calculated along the Horizontal Axis Z Using BUGLE-96	p. 107



di

118

3

Validation of the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 Cross Section Libraries on the PCA-Replica (Water/Iron) Neutron Shielding Benchmark Experiment

Massimo PESCARINI, Roberto ORSI, Manuela FRISONI

July 2014

1 - INTRODUCTION

The ENEA-Bologna Nuclear Data Group generated two broad-group coupled (47 n + 20 γ) working cross section libraries in FIDO-ANISN /1/ format, named BUGJEFF311.BOLIB /2/ and BUGENDF70.BOLIB /3/ and respectively based on the OECD-NEADB JEFF-3.1.1 /4/ (see also /5/) and US ENDF/B-VII.0 /6/ evaluated nuclear data libraries. The same neutron and photon energy group structure of the ORNL BUGLE-96 /7/ (ENDF/B-VI.3 /8/ evaluated nuclear data) working cross section library were adopted together with the same data format and processing methodology. All these ENEA-Bologna and ORNL libraries were specifically conceived for LWR shielding and pressure vessel dosimetry applications and contain problem-dependent parameterized sets of self-shielded cross sections specifically prepared for BWR and PWR applications. It was considered a meaningful test to validate the two ENEA-Bologna libraries and the ORNL library on the PCA-Replica /9/ (see also /10/) water/iron (H₂O/Fe) engineering neutron shielding benchmark experiment that reproduces the ex-core radial geometry of a PWR and is included in the SINBAD /11/ (see also /12/) international database of reactor shielding benchmark experiments. PCA-Replica is particularly fit to test the cited working libraries since it was specifically conceived to check the calculated fast neutron fluxes in a PWR mild steel pressure vessel simulator. The results obtained with the BUGLE-96 library represent a reliable reference comparison because this library was widely and successfully used all over the world in the previously cited applications since 1996. The three cited libraries were alternatively used in fixed source transport calculations performed in Cartesian (X,Y,Z) geometry with the TORT-3.2 /13/ three-dimensional (3D) discrete ordinates (S_N) code, included in the ORNL DOORS /14/ system of deterministic transport codes.

The neutron dosimeter cross sections used in the calculations were processed (see /15/) from the IAEA IRDF-2002 /16/ reactor dosimetry file. The ENEA-Bologna programs ADEFTA-4.1 /17/ and BOT3P-5.3 /18/ (see also /19/, /20/ and /21/) were respectively employed for the calculation of the isotopic atomic densities and for the automatic generation of the spatial mesh grid of the geometrical model. The calculated dosimetric and spectral integral results were compared with the corresponding experimental data, obtained using threshold activation dosimeters (Rh-103(n,n')Rh-103m, In-115(n,n')In-115m and S-32(n,p)P-32) for the dosimetric data and spherical hydrogen-filled proportional counters (type SP-2) together with a spherical organic liquid (NE213) scintillator for the spectral data.



2 - PCA-REPLICA EXPERIMENT

2.1 - PCA-Replica Experimental Facility

The PCA-Replica 12/13 low-flux engineering neutron shielding experiment /9//10/ (Winfrith, UK, 1984) is a water/iron (H₂O/Fe) benchmark experiment including two water layers alternated with a PWR thermal shield (TS) simulator and a PWR pressure vessel (RPV) simulator. The PCA-Replica experimental facility (see FIGs. 2.1 and 2.2) duplicated exactly the ex-core radial geometry of the ORNL PCA (Pool Critical Assembly) /22/ similar experiment (Oak Ridge, US, 1981), simulating the ex-core radial geometry of a PWR. In particular PCA-Replica reproduced (see FIG. 2.3) the 12/13 configuration of the PCA experiment with a layer of water of about 12 cm between the core and the thermal shield simulator and a layer of water of about 13 cm between the thermal shield simulator and the pressure vessel simulator. An important feature differentiated the two experiments: the lowflux reactor neutron source of the PCA experiment was replaced in the PCA-Replica experiment with a neutron source emitted by a thin fission plate containing highly enriched uranium with a rectangular cross-sectional area identical to that of the PCA reactor source. It is underlined that this simpler source configuration of the PCA-Replica experiment could more easily be calibrated with a high degree of accuracy, reducing in this way a possible cause of the in-vessel neutron flux underpredictions noted in transport analyses dedicated to the PCA experiment, despite the extensive work addressed to obtain an accurate calibration /23/.

As previously cited, the source of neutrons in the PCA-Replica experiment was a rectangular fission plate irradiated (see FIGs. 2.2 and 2.3) by the NESTOR reactor (30 kW at the maximum power) through a graphite thermal column (total thickness = 43.91 cm), in the ASPIS shielding facility (see FIG. 2.2). The thin fission plate (with dimensions $63.5 \times 40.2 \times 0.6$ cm) was made (see TAB. 2.1) of highly enriched uranium (93.0 w% in U-235) alloyed with aluminium. Beyond the fission plate, the Replica shielding array was arranged (see FIG. 2.2) in a large parallelepiped steel tank (square section; side 180.0 cm) filled with water and surrounded by a thick concrete shield. After the first water gap (12.1 cm thick) there was (see FIG. 2.3) the stainless steel thermal shield simulator and the second water gap (12.7 cm thick). Then the mild steel RPV simulator was located and tightly connected with a void box made of a thin layer of aluminium, simulating the air cavity between the RPV and the biological shield in a real PWR.

The fission plate (0.6 cm thick), the TS (5.9 cm thick), the RPV (thickness T = 22.5 cm) and the void box (29.58 cm thick) were perfectly orthogonally aligned and centred along the imaginary line Z (horizontal or nuclear axis) passing through the centroid of the fission plate (see FIGs. 2.3 and 2.6).

Along the horizontal nuclear axis Z, threshold activation neutron dosimeters and neutron spectrometers were located in all or in part of the ten measure spatial positions and gave respectively the dosimetric and spectral experimental results.

The dimensions and materials of the PCA-Replica 12/13 configuration are reported in TAB. 2.1 (derived from TAB. 2 of reference /9/) in 18 zones, along the horizontal nuclear axis Z. The material composition of the PCA-Replica experiment is shown in TAB. 2.2 (derived from TAB. 3 of reference /9/).





FIG. 2.1 The Shielding Facilities of the NESTOR Reactor^a.

(^a) Figure derived from FIG. 2 of reference /9/.





^(a) Figure derived from FIG. 3 of reference /9/.

di



FIG. 2.3

PCA-Replica - Layout of the 12/13 Configuration^a.



MATERIAL/20NE NUMBER Graphite: 1, 5. Aluminium: 2, 4, 7, 9, 10, 15, 17. Void (Air): 3, 6, 16. Alloy Fuel (Fission Plate): 8. Water: 11, 13, 18. Stainless Steel: 12. Mild Steel: 14, 20, 21. Concrete: 19.

(^a) Figure derived from FIG. 5 of reference /9/.



TAB. 2.1

Zone	Material	Section	Dimensions	[cm]
1	Carbon	Square	119	Side
2	Aluminium	Square	119	Side
3	Void	Square	185	Side
4	Aluminium	Circular	56.06	Radius
5	Carbon	Square	180	Side
6	Void	Square	180	Side
7	Aluminium	Rectangular	68.5 × 47.5	
8	Fuel	Rectangular	63.5×40.2	
9	Aluminium	Rectangular	68.5 × 47.5	
10	Aluminium	Square	180	Side
11	Water	Square	180	Side
12	Stainless Steel	Square	68.5	Side
13	Water	Square	180	Side
14	Mild Steel	Square	68.5	Side
15	Aluminium	Square	60	Side
16	Void	Square	59.4	Side
17	Aluminium	Square	60	Side
18	Water	Square	180	Side
		1		

PCA-Replica - Dimensions and Materials.

Notes:

- (1) The sides of the trolley are nominally 2.54 cm of steel and outside this steel and the coupling stack zones 1 and 2 (see FIG. 2.3) there is concrete.
- (2) The aluminium plate zone 10 (see FIG. 2.3) is attached to a 1.91 cm thick steel plate which forms the front of the large water tank housing the PCA-Replica equipment. There is a 55.88 cm radius hole cut through the plate as shown in FIG. 2.2.
- (3) The Z axial dimension of zone 8 shown in FIG. 2.3, 0.6 cm, is set to allow for four layers of alloy fuel each 0.1016 cm thick. The alloy fuel density is $3.257 \text{ g} \times \text{cm}^{-3}$ and to allow for the clearance gaps this should be reduced to $2.206 \text{ g} \times \text{cm}^{-3}$.



TAB. 2.2

Material	Material Density $[g \times cm^{-3}]$	Element	Weight [%]	Atomic Density [atoms \times cm ⁻³]
Graphite	1.65	С	100.0	8.276E+22
Aluminium Cladding	2.70	Al	100.0	6.029E+22
Alloy Fuel (^a)	3.257	Al U-235 U-238	80.0 18.6 1.4	5.818E+22 1.552E+21 1.154E+20
Water	1.0	H O	11.19 88.81	6.688E+22 3.344E+22
Stainless Steel	7.88	C Si Mn P S Cr Ni Mo Ti Nb Cu Fe	$\begin{array}{c} 0.017\\ 0.44\\ 1.57\\ 0.025\\ 0.006\\ 18.4\\ 9.4\\ 0.37\\ 0.009\\ 0.014\\ 0.24\\ 69.509\end{array}$	6.721E+19 7.438E+20 1.356E+21 3.832E+19 8.884E+18 1.688E+22 7.601E+21 1.831E+20 8.920E+18 7.154E+18 1.793E+20 5.909E+22
Mild Steel	7.835	C Mn P S Fe	0.22 1.09 0.01 0.032 98.648	8.646E+20 9.366E+20 1.524E+19 4.711E+19 8.338E+22
Concrete	2.3	Si Fe H O Al Ca Na K	33.7 1.4 1.0 52.9 3.4 4.4 1.6 1.6	4.120E+22 8.609E+20 3.407E+22 1.135E+23 4.327E+21 3.770E+21 2.390E+21 1.405E+21

PCA-Replica - Material Composition.

(^a) Uranium enriched to 93 w % in U-235.



2.2 - PCA-Replica Fission Plate

The PCA-Replica experiment was driven by the neutron source emitted from a fission plate coupled to the NESTOR reactor core via a graphite thermal column (see 2.1). The fission rate spatial distribution throughout the fission plate was required to provide a source of adequate spatial resolution for neutronic transport calculations.

As reported on page 43 of reference /9/, the fission plate was constructed of 52 uranium aluminium alloy fuel strips of height 635 mm, width 30.48 mm and thickness 1.016 mm. The strips of density 3.257 g × cm⁻³ were 80% by weight of Al and 20% by weight of U enriched to 93 w % in U-235. Sets of 4 fuel strips were laid on top of each other and 13 of these assemblies were placed side by side on a pitch of 30.92 mm to form the fuel structure of the fission plate. This structure (see zone 8 of FIG. 2.3) was enclosed in a thin aluminium envelope (see zones 7 and 9 of FIG. 2.3).

The fission plate detail is schematically shown in FIG. 2.4 (derived from FIG. A1 of reference /9/) whereas the fuel tablet arrangement in a fission plate element is described in FIG. 2.5 (derived from FIG. A11 of reference /9/).

The co-ordinate system used throughout the present analysis is the same as that reported in the FIG. 5 of reference /9/. The front of the fission plate is defined as the face closest to the core of the NESTOR reactor. The Z axis is from the NESTOR core through the centre of the rectangular fission plate, as shown in FIG. 2.6 (derived from FIG. A2 of reference /9/). The origin of the co-ordinate system (0.0, 0.0, 0.0) is positioned at the centre of the back face (see FIG. 2.6) of the thin aluminium envelope of the fission plate, as indicated also in FIG. 2.3 (derived from FIG. 5 of reference /9/). The X and Y axes together with the Z axis define respectively the horizontal and vertical planes across the fission plate.

Finally, the PCA-Replica neutron source strength spatial distribution (5×11 source mesh) per Watt of plate power in the 0.6 cm thick fission plate is reported in TAB. 2.3 (derived from TAB. A6 of reference /9/).





PCA-Replica - Detail of the Fission Plate Fabricated in Aluminium^{a,b}.



(^a) Figure derived from FIG. A1 of reference /9/.

(^b) The numerical value of the alloy fuel density $(3.256 \text{ g} \times \text{cm}^{-3})$ reported in the present figure is slightly different from the value $(3.257 \text{ g} \times \text{cm}^{-3})$ shown in the TABs. 2.1 and 2.2 and assumed in the calculations.



PCA-Replica - Fuel Tablet Arrangement in a Fission Plate Element^a.



(^a) Figure derived from FIG. A11 of reference /9/.



PCA-Replica - Co-Ordinate System^{a,b}.



- ^(a) Figure derived from FIG. A2 of reference /9/.
- ^(b) The origin of the X, Y and Z axes in the reference system adopted is located in the centre of the back face of the fission plate inclusive of the thin aluminium envelope, as shown also in FIG. 2.3.



TAB. 2.3

PCA-Replica - Neutron Source Strength Spatial Distribution (5×11 Mesh) in the 0.6 cm Thick Fission Plate^a.

[neutrons \times cm ⁻³ \times s ⁻¹ \times Plate Watt ⁻¹]						
X-axis [cm] [cm]	-20.10 ÷ 12.10	-12.10 ÷ -4.10	-4.10 ÷ 4.10	4.10 ÷ 12.10	12.10 ÷ 20.10	
-31.75 ÷ -26.32	4.424E+07	4.418E+07	4.495E+07	4.448E+07	4.560E+07	
-26.32 ÷ -20.58	4.609E+07	4.518E+07	4.557E+07	4.535E+07	4.772E+07	
-20.58 ÷ -15.44	4.885E+07	4.696E+07	4.744E+07	4.747E+07	5.040E+07	
-15.44 ÷ -10.00	5.157E+07	4.885E+07	4.690E+07	4.989E+07	5.293E+07	
-10.00 ÷ -3.33	5.393E+07	5.055E+07	5.160E+07	5.217E+07	5.505E+07	
-3.33 ÷ 3.33	5.500E+07	5.135E+07	5.252E+07	5.332E+07	5.601E+07	
3.33 ÷ 10.00	5.426E+07	5.078E+07	5.179E+07	5.264E+07	5.531E+07	
10.00 ÷ 15.44	5.231E+07	4.927E+07	4.996E+07	5.069E+07	5.351E+07	
15.44 ÷ 20.58	5.006E+07	4.764E+07	4.806E+07	4.855E+07	5.144E+07	
20.58 ÷ 26.32	4.802E+07	4.642E+07	4.684E+07	4.699E+07	4.964E+07	
26.32 ÷ 31.75	4.723E+07	4.670E+07	4.778E+07	4.756E+07	4.874E+07	

Note: 1 Watt = $3.121E+10 \times 2.437$ [neutrons × s⁻¹].

(^a) Table derived from TAB. A6 of reference /9/.



2.3 - PCA-Replica Experimental Measures

The threshold activation dosimeters used in the PCA-Replica 12/13 experiment along the horizontal nuclear axis Z were Rh-103(n,n')Rh-103m, In-115(n,n')In-115m and S-32(n,p)P-32.

The Rh-103(n,n') dosimeters were located in the ten measure positions while the In-115(n,n') and S-32(n,p) dosimeters were used only in the following three measure positions: in the 1/4 T and 3/4 T positions in the RPV simulator and in the void box position.

The "as measured" experimental reaction rates of the dosimeters must be reduced (see page 10 of reference /9/) by 4% in the RPV and void box measure positions and by 2% in the measure positions located in the water gaps to correct for the presence of the NESTOR core neutron leakage background.

The reaction threshold energies for the Rh-103(n,n'), In-115(n,n') and S-32(n,p) dosimeters, in a light water material testing reactor (MTR) spectrum similar to that of the PCA-Replica experiment, are respectively 0.04, 0.34 and 0.95 MeV while the effective threshold energies are 0.69, 1.30 and 2.7 MeV (see /24/). Nevertheless, since the effective threshold is not a complete satisfactory parameter for the characterization of the energy dependent cross section functions, the present values give only a rough indication of the start of the response for the specific dosimeter. If one wishes to characterize the dosimeter response energy range more accurately, the energy range corresponding to 90% of the response and the median energy of the response should be taken into account. The median energy is defined such that, in the specific spectrum, the responses below and above this energy numerical value are equal. Secondly, the definition of the energy range corresponding to 90% of the total response of a dosimeter implies that 5% of the response is below the lower boundary and 5% above the upper boundary of this energy range. A synthesis of these data for the three dosimeters used in the PCA-Replica experiment is reported in TAB. 2.4 to give more specific detailed information addressed to obtain a more precise analysis in the comparison of the experimental and calculated dosimetric results.

TAB. 2.4

PCA-Replica - Dosimeter Parameters in a Light Water MTR Neutron Spectrum. (see /24/)

Dosimeter	Effective Energy Threshold [MeV]	90% Response Energy Range [MeV]	Median Energy [MeV]
Rh-103(n,n')	0.69	0.53 - 5.4	1.9
In-115(n,n')	1.30	1.0 - 5.6	2.4
S-32(n,p)	2.70	2.2 - 7.4	3.9

In practice the experimental results coming from Rh-103(n,n') and In-115(n,n') (see /25/) correspond to neutron fluxes above about 1.0 MeV and the esperimental results from S-32(n,p) with neutron fluxes above about 3.0 MeV.



The spectral measures in the PCA-Replica 12/13 experiment were performed only in two positions (see FIG. 2.3): in the 1/4 T (Z = 39.01 cm) position of the mild steel pressure vessel simulator and in the void box (Z = 58.61 cm) filled with air. As reported in reference /9/, two kinds of spectrometer were used. The spherical hydrogen-filled proportional counters employed were of type SP-2 of internal diameter 40.0 mm. Individual counters with gas fillings of approximately 0.5, 1.0, 3.0 and 10.0 atmospheres were used in combination, to cover the energy range from 50.0 keV to 1.2 MeV. The neutron fluxes between 1.0 and 10.0 MeV were determined with a spherical 3.5 ml organic liquid (NE213) scintillator.

The experimental neutron spectrum data taken in the two previously cited measure positions are shown in TAB. 2.5 (derived from TAB. 7 of reference /9/): the reported spectral data are given "as measured", i.e. the NESTOR core neutron leakage background of 4% has not been removed.

The complete experimental details concerning the PCA-Replica 12/13 benchmark experiment are reported in reference /9/.



TAB. 2.5

PCA-Replica - Experimental Neutron Spectra as Measured in the 1/4 T RPV Position and in the Void Box Position.

Neutron Energy Group Boundaries	Lethargy Width	Neutron Flux Per Unit Lethargy / NESTOR Reactor Watt	
		Voided 1/4 T RPV	Void Box
0.052 - 0.059 0.059 - 0.067 0.067 - 0.076 0.076 - 0.086 0.086 - 0.097 0.097 - 0.111 0.111 - 0.126 0.126 - 0.143 0.143 - 0.162 0.162 - 0.183 0.183 - 0.207 0.207 - 0.235 0.235 - 0.266 0.266 - 0.302 0.302 - 0.342 0.342 - 0.388 0.388 - 0.439 0.439 - 0.498 0.498 - 0.564 0.564 - 0.639	$\begin{array}{c} 0.126\\ 0.127\\ 0.126\\ 0.124\\ 0.120\\ 0.135\\ 0.127\\ 0.125\\ 0.122\\ 0.123\\ 0.122\\ 0.123\\ 0.127\\ 0.124\\ 0.127\\ 0.124\\ 0.126\\ 0.123\\ 0.126\\ 0.124\\ 0.125\\ \end{array}$	6.8 6.0 6.7 6.7 6.3 7.4 9.0 10.0 9.0 10.0 9.0 10.0 9.0 10.0 9.2 10.3 11.7 14.0 17.0 16.0 13.7 16.2 19.0 23.9 10.0 23.9 10.0 11.7 14.0 17.0 16.0 13.7 16.2 19.0 23.9 23.9 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0	Void Box 0.45 0.68 1.21 1.15 0.58 0.87 1.48 2.22 1.62 1.92 1.60 1.49 2.22 3.13 3.31 2.99 1.88 2.33 2.74 4.12
0.639 - 0.724 0.724 - 0.821 0.821 - 0.930 0.930 - 1.054 1.054 - 1.194 1.194 - 1.353 1.353 - 1.534 1.534 - 1.738 1.738 - 1.969 1.969 - 2.231 2.231 - 2.528 2.528 - 2.865 2.865 - 3.246 3.246 - 3.679 3.679 - 4.169 4.169 - 4.724 4.724 - 5.353 5.353 - 6.065 6.065 - 6.873 6.873 - 7.788 7.788 - 8.825 8.825 - 10.0	$\begin{array}{c} 0.125\\ 0.126\\ 0.125\\ 0.$	$\begin{array}{c} 20.3 \\ 17.1 \\ 15.7 \\ 15.5 \\ 15.3 \\ 13.7 \\ 13.8 \\ 13.3 \\ 11.9 \\ 11.7 \\ 11.2 \\ 9.2 \\ 6.9 \\ 4.4 \\ 4.8 \\ 5.0 \\ 4.2 \\ 3.5 \\ 2.2 \\ 1.5 \\ 1.1 \\ 0.2 \end{array}$	3.19 1.75 1.93 1.69 1.53 1.16 0.94 0.78 0.61 0.46 0.35 0.27 0.18 0.13 0.10 0.09 0.09 0.09 0.07 0.06 0.03 0.02



3 - CROSS SECTION LIBRARIES AND NUCLEAR DATA

The group working cross section libraries (BUGJEFF311.BOLIB /2/, BUGENDF70.BOLIB /3/ and BUGLE-96 /7/) and the nuclear data (the IRDF-2002 /16/ derived reactor dosimetry cross sections /15/ and the JEFF-3.1.1, ENDF/B-VII.0 and ENDF/B-VI.3 U-235 fission neutron spectra in the BUGLE-96 neutron group structure) used in the present deterministic transport analysis are briefly described in this chapter. It is underlined that the ENEA-Bologna BUGJEFF311.BOLIB and BUGENDF70.BOLIB libraries adopted the same neutron (see TAB. 3.1) and photon (see TAB. 3.2) group structure of the ORNL BUGLE-96 library.

3.1 - BUGJEFF311.BOLIB Cross Section Library

BUGJEFF311.BOLIB /2/ is an ENEA-Bologna broad-group (47 neutron groups + 20 photon groups) coupled neutron and photon working cross section library in FIDO-ANISN format, generated in the same energy group structure of the ORNL BUGLE-96 /7/ similar library and based on the OECD-NEADB JEFF-3.1.1 /4/ /5/ evaluated nuclear data library. This library was obtained through problem-dependent cross section collapsing and self-shielding from the ENEA-Bologna VITJEFF311.BOLIB /26/ fine-group coupled neutron and photon pseudo-problem-independent library in AMPX format for nuclear fission applications. VITJEFF311.BOLIB adopts the same energy group structure (199 neutron groups + 42 photon groups) of the ORNL VITAMIN-B6 /7/ library and it is based on the Bondarenko /27/ (f-factor) neutron resonance self-shielding method.

BUGJEFF311.BOLIB, dedicated to LWR shielding and pressure vessel dosimetry applications, was generated with the ENEA-Bologna 2007 Revision /28/ of the ORNL SCAMPI /29/ nuclear data processing system, able to treat double precision data and freely released at OECD-NEADB and ORNL-RSICC.

The BUGJEFF311.BOLIB library was freely released at OECD-NEADB in 2011, assuming the designation NEA-1866 ZZ BUGJEFF311.BOLIB.

3.2 - BUGENDF70.BOLIB Cross Section Library

BUGENDF70.BOLIB /3/ is an ENEA-Bologna broad-group (47 neutron groups + 20 photon groups) coupled neutron and photon working cross section library in FIDO-ANISN format, generated in the same energy group structure of the ORNL BUGLE-96 /7/ similar library and based on the US ENDF/B-VII.0 /6/ evaluated nuclear data library. This library was obtained through problem-dependent cross section collapsing and self-shielding from the ENEA-Bologna VITENDF70.BOLIB /30/ fine-group coupled neutron and photon pseudo-problem-independent library in AMPX format for nuclear fission applications. VITENDF70.BOLIB adopts the same energy group structure (199 neutron groups + 42 photon groups) of the ORNL VITAMIN-B6 /7/ library and it is based on the Bondarenko /27/ (f-factor) neutron resonance self-shielding method.

BUGENDF70.BOLIB, dedicated to LWR shielding and pressure vessel dosimetry applications, was generated with the ENEA-Bologna 2007 Revision /28/ of the ORNL SCAMPI /29/ nuclear data processing system, able to treat double precision data and freely released at OECD-NEADB and ORNL-RSICC.

The BUGENDF70.BOLIB library was freely released at OECD-NEADB in 2013, assuming the designation NEA-1872 ZZ BUGENDF70.BOLIB.



3.3 - BUGLE-96 Cross Section Library

BUGLE-96 /7/ is an ORNL broad-group (47 neutron groups + 20 photon groups) coupled neutron and photon working cross section library in FIDO-ANISN format, based on the US ENDF/B-VI.3 /8/ evaluated nuclear data library. BUGLE-96 was obtained through problem-dependent cross section collapsing and self-shielding from the ORNL VITAMIN-B6 /7/ fine-group (199 neutron groups + 42 photon groups) coupled neutron and photon pseudo-problem-independent library in AMPX format for nuclear fission applications. VITAMIN-B6 is based on the Bondarenko /27/ (f-factor) neutron resonance self-shielding method.

BUGLE-96, dedicated to LWR shielding and pressure vessel dosimetry applications, was generated with the ORNL SCAMPI /29/ nuclear data processing system and was freely released to OECD-NEADB in 1996 where assumed the designation DLC-0185 ZZ BUGLE-96. It is underlined that BUGLE-96, together with the mother library VITAMIN-B6, became reference standards (see /31/, ANSI/ANS-6.1.2-1999 (R2009)) as multi-group libraries for shielding applications and they were successfully used all over the world.



Neutron Group Energy and Lethargy Boundaries for the BUGLE-96 Library.

Group	Upper Energy [eV]	Upper Lethargy
1	1 73325-07	-5 49978-01
2	1 4191E+07	-3.5002E-01
3	1 2214E+07	-2 0000E-01
4	1.0000E+07	0.
- 5	8.6071E+06	1.5000E-01
6	7.4082E+06	3.0000E-01
7	6.0653E+06	5.0000 = 01
8	4.9659E+06	7.0000E-01
9	3.6788E+06	1.0000E-00
10	3.0119E+06	1.2000E+00
11	2.7253E+06	1.3000E+00
12	2.4660E+06	1.4000E+00
13	2.3653E+06	1.4417E+00
14	2.3457E+06	1.4500E+00
15	2.2313E+06	1.5000E+00
16	1.9205E+06	1.6500E+00
17	1.6530E+06	1.8000E+00
18	1.3534E+06	2.0000E+00
19	1.0026E+06	2.3000E+00
20	8.2085E+05	2.5000E+00
21	7.4274E+05	2.6000E+00
22	6.0810E+05	2.8000E+00
23	4.9787E+05	3.0000E+00
24	3.6883E+05	3.3000E+00
25	2.9721E+05	3.5159E+00
26	1.8316E+05	4.0000E+00
27	1.1109E+05	4.5000E+00
28	6.7379E+04	5.0000E+00
29	4.0868E+04	5.5000E+00
30	3.1828E+04	5.7500E+00
31	2.6058E+04	5.9500E+00
32	2.4176E+04	6.0250E+00
33	2.1875E+04	6.1250E+00
34	1.5034E+04	6.5000E+00
35	7.1017E+03	7.2500E+00
36	3.3546E+03	8.0000E+00
37	1.5846E+03	8.7500E+00
38	4.5400E+02	1.0000E+01
39	2.1445E+02	1.0750E+01
40	1.0130E+02	1.1500E+01
41	3.7266E+01	1.2500E+01
42	1.0677E+01	1.3750E+01
43	5.0435E+00	1.4500E+01
44	1.8554E+00	1.5500E+01
45	8.7643E-01	1.6250E+01
46	4.1399E-01	1.7000E+01
47	1.0000E-01	1.8421E+01
	1.0000E-05	2.7631E+01



Photon Group Energy Boundaries for the BUGLE-96 Library.

Group	Upper Energy [eV]	
1	1.4000E+07	
2	1.0000E+07	
3	8.0000E+06	
4	7.0000E+06	
5	6.0000E+06	
6	5.0000E+06	
7	4.0000E+06	
8	3.0000E+06	
9	2.0000E+06	
10	1.5000E+06	
11	1.0000E+06	
12	8.0000E+05	
13	7.0000E+05	
14	6.0000E+05	
15	4.0000E+05	
16	2.0000E+05	
17	1.0000E+05	
18	6.0000E+04	
19	3.0000E+04	
20	2.0000E+04	
	1.0000E+04	



3.4 - IRDF-2002 Dosimeter Cross Sections

The threshold activation dosimeter cross sections used in the transport calculations were all derived (see /15/) from the IAEA International Reactor Dosimetry File 2002 /16/ (IRDF-2002). A major objective of this data development project was to prepare and distribute a standardized, updated and tested reactor dosimetry cross section library accompanied by uncertainty information for use in service life assessments of nuclear power reactors.

In particular the Rh-103(n,n')Rh-103m, In-115(n,n')In-115m and S-32(n,p)P-32 dosimeter cross sections needed in the PCA-Replica transport analyses with the ENEA-Bologna BUGJEFF311.BOLIB /2/ and BUGENDF70.BOLIB /3/ cross section libraries were taken respectively from the corresponding library packages. These data were derived from the IRDF-2002 set of point-wise dosimetry cross sections through proper data processing with the GROUPIE program of the PREPRO 2007 /32/ nuclear data processing system into the BUGJEFF311.BOLIB and BUGENDF70.BOLIB 47-group neutron energy structure, identical to that of the ORNL BUGLE-96 /7/ cross section library. These dosimeter cross sections were obtained (see /15/) using two cross section weightings ("flat weighting" and "1/4 T RPV weighting") in the 199-group neutron energy structure of the ORNL VITAMIN-B6 /7/ library, libraries BUGJEFF311.BOLIB adopted bv the fine-group mother of and BUGENDF70.BOLIB, i.e. by VITJEFF311.BOLIB /26/ and VITENDF70.BOLIB /30/ respectively. In particular the 1/4 T RPV neutron weighting spectra were obtained at the onequarter thickness (T) position of the pressure vessel of a typical PWR, through problemdependent one-dimensional transport calculations using alternatively the VITJEFF311.BOLIB (see TAB. 3.4 of reference /2/) and VITENDF70.BOLIB (see TAB. 3.4 of reference /3/) libraries. Concerning the IRDF-2002 1/4 T RPV weighting neutron dosimeter cross sections used in the transport calculations with BUGLE-96, they were obtained for the present transport analysis with the same calculation procedure previously described, using the 1/4 T RPV neutron weighting spectrum (see TAB. 3.4 of reference /7/) calculated at ORNL with the VITAMIN-B6 fine-group mother library of BUGLE-96.

It is underlined that, for the same specific dosimeter, the group numerical values of each flat weighting cross section set in the BUGLE-96 47-group neutron energy structure are obviously identical for all the three BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 libraries used in the transport calculations.

The flat weighting 47-group cross sections for the three Rh-103(n,n')Rh-103m, In-115(n,n')In-115m and S-32(n,p)P-32 dosimeters, used together with all the three cited working cross section libraries, are reported in TAB. 3.3 and their corresponding graphical representations are respectively shown in FIGs. 3.1, 3.2 and 3.3.

The 1/4 T RPV weighting 47-group cross sections for the three Rh-103(n,n')Rh-103m, In-115(n,n')In-115m and S-32(n,p)P-32 dosimeters are respectively reported in the TABs. 3.4, 3.5 and 3.6, respectively for the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 cross section libraries.



```
FIG. 3.1
```







```
FIG. 3.2
```







```
FIG. 3.3
```

IRDF-2002 Flat Weighting S-32(n,p)P-32 Dosimeter Cross Sections in the BUGLE-96 47-Group Neutron Energy Structure.





IRDF-2002 Flat Weighting Neutron Dosimeter Cross Sections [barns] Used in the TORT-3.2 Calculations with BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96.

Group	Upper Energy	Rh-103	In-115	S-32
Group	[MeV]	(n,n')	(n,n')	(n,p)
1	1.7332E+01	2.3466E-01	5.8133E-02	1.7639E-01
2	1.4191E+01	3.8742E-01	9.1680E-02	3.0787E-01
3	1.2214E+01	8.1816E-01	2.0239E-01	3.8051E-01
4	1.0000E+01	1.2190E+00	2.7381E-01	3.3979E-01
5	8.6071E+00	1.2753E+00	3.0859E-01	3.2202E-01
6	7.4082E+00	1.2305E+00	3.3417E-01	3.1380E-01
7	6.0653E+00	1.1732E+00	3.3897E-01	2.4629E-01
8	4.9659E+00	1.1091E+00	3.2538E-01	2.7592E-01
9	3.6788E+00	1.0370E+00	3.3341E-01	1.9108E-01
10	3.0119E+00	9.8735E-01	3.5259E-01	1.0053E-01
11	2.7253E+00	9.5185E-01	3.5385E-01	6.8686E-02
12	2.4660E+00	9.2536E-01	3.4311E-01	7.2417E-02
13	2.3653E+00	9.1570E-01	3.3654E-01	6.6472E-02
14	2.3457E+00	9.0494E-01	3.2759E-01	6.1245E-02
15	2.2313E+00	8.6764E-01	2.9012E-01	2.1377E-02
16	1.9205E+00	8.0955E-01	2.3022E-01	4.1502E-03
17	1.6530E+00	7.4452E-01	1.7096E-01	5.9998E-04
18	1.3534E+00	6.6193E-01	1.0336E-01	6.0917E-05
19	1.0026E+00	5.8044E-01	4.9401E-02	1.6785E-06
20	8.2085E-01	4 .9269E-01	2.7891E-02	0.
21	7.4274E-01	3.3867E-01	1.5489E-02	0.
22	6.0810E-01	1.9319E-01	6.3893E-03	0.
23	4.9787E-01	1.3801E-01	2.2558E-03	0.
24	3.6883E-01	1.0374E-01	1.6310E-04	0.
25	2.9721E-01	6.6383E-02	0.	0.
26	1.8316E-01	2.3291E-02	0.	0.
27	1.1109E-01	5.8219E-03	0.	0.
28	6.7379E-02	1.6581E-03	0.	0.
29	4.0868E-02	3.4572E-06	0.	0.
30	3.1828E-02	0.	0.	0.
31	2.6058E-02	0.	0.	0.
32	2.4176E-02	0.	0.	0.
33	2.1875E-02	0.	0.	0.
34	1.5034E-02	0.	0.	0.
35	7.1017E-03	0.	0.	0.
36	3.3546E-03	0.	0.	0.
37	1.5846E-03	0.	0.	0.
38	4.5400E-04	0.	0.	0.
39	2.1445E-04	0.	0.	0.
40	1.0130E-04	0.	0.	0.
41	3.7266E-05	0.	0.	0.
42	1.0677E-05	0.	0.	0.
43	5.0435E-06	0.	0.	0.
44	1.8554E-06	0.	0.	0.
45	8.7643E-07	0.	0.	0.
46	4.1399E-07	0.	0.	0.
47	1.0000E-07	0.	0.	0
	1.0000E-11			



IRDF-2002 1/4 T RPV Weighting Neutron Dosimeter Cross Sections [barns] Used in the TORT-3.2 Calculations with the BUGJEFF311.BOLIB Library.

GroupUpper Energy [MeV]Rh-103 (n,n')In-115 (n,n')S-32 (n,p)11.7332E+012.4762E-015.9192E-021.9546E-0121.4191E+014.0937E-019.8480E-023.1934E-0131.22148+018.6632E-012.1539E-013.7676E-0141.0000E+011.2744E+003.1011E-013.2276E-0158.6071E+001.2242E+003.3546E-012.1475E-0167.4082E+001.079E+003.2516E-012.4085E-0176.0653E+001.1079E+003.2568E-011.0010E-01103.0119E+009.8700E-013.5268E-011.0010E-01112.7253E+009.1570E-013.5268E-011.0010E-01122.4650E+009.1570E-013.3548E-016.6656E-02132.3653E+009.1570E-013.3548E-016.1061E-02142.34578+009.1570E-013.3548E-016.1061E-02152.2313E+008.0741E-012.8968E-013.1776E-02161.9205E+005.7702E-014.7963E-020.171.6530E+007.7225E-011.6338E-015.7668E-04181.3534E+006.5961E-011.0148E-015.6340E-05191.0026E+005.7702E-014.7963E-020.226.0810E-011.3327E-011.4938E-020.234.9778E-011.3327E-011.4938E-020.243.6683E-012.1485E-020.0.252.9721E-016.5592					
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$		Upper Energy	Rh-103	In-115	s-32
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Group	[MeV]	(n,n')	(n,n')	(n,p)
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$					
2 1.4191E+01 4.0937E-01 9.84802-02 3.1934E-01 3 1.2214E+01 8.663E-01 2.1538E-01 3.7876E-01 4 1.000DE+01 1.2274E+00 3.1011E-01 3.276E-01 5 8.6071E+00 1.2744E+00 3.011E-01 3.2776E-01 7 6.0653E+00 1.173E+00 3.366E-01 2.1766E-01 8 4.9659E+00 1.0344E+00 3.3464E-01 2.4085E-01 9 3.678E+00 1.0344E+00 3.3464E-01 1.8725E-01 10 3.0119E+00 9.8700E-01 3.526E-01 1.6656E-02 12 2.4660E+00 9.2492E-01 3.4233E-01 7.2333E-02 13 2.3457E+00 9.6468E-01 3.2736E-01 6.6747E-02 14 2.3457E+00 9.468E-01 3.2736E-01 2.176E-02 15 2.2313E+00 8.6738E-01 1.6934E-01 5.068E-04 16 1.9205E+00 8.741E-01 1.6934E-01 5.0648E-04 17 1.6530E+01 7.1693E-02 0. 0. 21 7.4274E-01 3.2977E-01 1.493	1	1.7332E+01	2.4762E-01	5.9192E-02	1.9546E-01
3 1.2214E+01 8.6632E-01 2.1539E-01 3.7876E-01 4 1.0000E+01 1.2276E+00 2.7596E-01 3.2762E-01 5 8.6071E+00 1.2276E+00 3.5346E-01 3.2276E-01 6 7.4082E+00 1.2262E+00 3.5346E-01 3.1147E-01 7 6.0653E+00 1.1713E+00 3.23546E-01 2.4085E-01 8 4.9659E+00 1.079E+00 3.2516E-01 2.760E-01 9 3.6786E+00 9.8700E-01 3.5268E-01 1.0010E-01 11 2.7253E+00 9.5196E-01 3.5387E-01 6.8656E-02 12 2.4660E+00 9.2492E-01 3.23654E-01 6.6472E-02 13 2.3653E+00 9.1570E-01 3.2865E-01 2.1076E-02 14 2.3457E+00 8.6739E-01 2.8986E-01 2.1176E-02 15 2.2313E+00 8.6739E-01 2.8986E-01 5.7068E-04 18 1.3534E+00 6.5961E-01 1.0488E-01 5.640E-05 19 1.0026E+00 7.702E-01 4.9638E-02 0. 21 7.4274E-01 1.3615E-01 <td>2</td> <td>1.4191E+01</td> <td>4.0937E-01</td> <td>9.8480E-02</td> <td>3.1934E-01</td>	2	1.4191E+01	4.0937E-01	9.8480E-02	3.1934E-01
4 1.0000E+01 1.2276E+00 2.7596E-01 3.3761E-01 5 8.6071E+00 1.2744E+00 3.1011E-01 3.2276E-01 7 6.0653E+00 1.1273E+00 3.33669E-01 2.4085E-01 7 6.0653E+00 1.079E+00 3.3444E-01 2.4085E-01 9 3.6788E+00 1.0344E+00 3.3444E-01 1.6725E-01 10 3.0119E+00 9.8700E-01 3.5268E-01 1.6725E-01 12 2.4660E+00 9.2492E-01 3.4283E-01 6.66472E-02 13 2.3653E+00 9.1570E-01 3.3526E-01 2.176E-02 14 2.3457E+00 9.0466E-01 3.2736E-01 6.1061E-02 15 2.2313E+00 8.6739E-01 2.8986E-01 2.1176E-02 16 1.9205E+00 8.7702E-01 1.6934E-01 5.6340E-05 19 1.0026E+00 5.7702E-01 4.7963E-02 0. 20 8.2085E-01 4.9153E-01 2.7146E-02 0. 21 7.4274E-01 1.6330E+02 0. 0. 22 6.0810E-01 1.9395E-01 6.4499E-	3	1.2214E+01	8.8683E-01	2.1539E-01	3.7876E-01
5 8.6071E+00 1.2748E+00 3.1011E-01 3.2276E-01 6 7.4082E+00 1.2262E+00 3.3546E-01 2.4085E-01 7 6.0633E+00 1.1713E+00 3.2516E-01 2.4085E-01 8 4.9659E+00 1.0348E+00 3.2448E-01 1.8725E-01 10 3.0119E+00 9.8700E-01 3.5268E-01 1.0010E-01 11 2.7253E+00 9.1596E-01 3.5268E-01 1.0010E-01 12 2.4660E+00 9.2492E-01 3.4283E-01 7.2333E-02 13 2.3653E+00 9.1570E-01 3.654E-01 6.6472E-02 14 2.3457E+00 9.04668E-01 3.2736E-01 6.161E-02 15 2.2313E+00 8.6739E-01 2.8986E-01 2.1176E-02 16 1.9205E+00 7.4261E-01 1.6934E-01 5.7068E-04 18 1.3534E+00 6.5961E-01 1.0148E-02 0. 20 8.2085E-01 4.9153E-01 2.1978E-02 0. 21 7.4274E-01 1.63362E-02 0. </td <td>4</td> <td>1.0000E+01</td> <td>1.2278E+00</td> <td>2.7598E-01</td> <td>3.3761E-01</td>	4	1.0000E+01	1.2278E+00	2.7598E-01	3.3761E-01
6 7.4082E+00 1.2262E+00 3.3546E-01 3.1147E-01 7 6.0653E+00 1.1713E+00 3.2516E-01 2.4085E-01 9 3.6788E+00 1.0344E+00 3.3444E-01 1.8725E-01 10 3.0119E+00 9.3448E-01 1.8725E-01 1.0010E-01 11 2.753E+00 9.5196E-01 3.5387E-01 6.8656E-02 12 2.4660E+00 9.2492E-01 3.4283E-01 7.2333E-02 13 2.3553E+00 9.1570E-01 3.3546E-01 6.6472E-02 14 2.3457E+00 9.0466E-01 3.2736E-01 6.1061E-02 15 2.2313E+00 8.6739E-01 2.896E-01 3.64470E-03 17 1.6530E+00 7.742E-01 1.0934E-01 5.6402-05 19 1.0026E+00 5.7702E-01 4.7963E-02 0. 21 7.4274E-01 3.2977E-01 1.4398E-02 0. 22 6.08102E-01 2.1316E-03 0. 0. 23 4.9787E-01 1.3615E-01 2.1316E-03	5	8.6071E+00	1.2744E+00	3.1011E-01	3.2276E-01
7 6.0653E+00 1.1713E+00 3.3669E-01 2.4085E-01 8 4.9659E+00 1.0344E+00 3.2516E-01 2.7606E-01 9 3.6788E+00 1.0344E+00 3.2516E-01 2.7606E-01 10 3.0119E+00 9.8700E-01 3.5268E-01 1.0010E-01 11 2.253E+00 9.1570E-01 3.3654E-01 6.865E-02 12 2.4660E+00 9.2492E-01 3.4283E-01 7.2333E-02 13 2.3653E+00 9.1570E-01 3.3564E-01 6.1061E-02 14 2.3457E+00 8.6739E-01 2.8986E-01 2.1176E-02 16 1.9205E+00 8.6741E-01 2.8986E-01 3.470E-03 17 1.6530E+00 7.4261E-01 1.6934E-01 5.6340E-05 19 1.0026E+00 5.7702E-01 1.703E-02 0. 20 8.2085E-01 4.9153E-01 2.7146E-02 0. 21 7.4274E-01 3.2377E-02 0. 0. 22 6.010E-01 1.9398E-01 2.1316E-03	6	7.4082E+00	1.2262E+00	3.3546E-01	3.1147E-01
8 4.9659E+00 1.1079E+00 3.2516E-01 2.7606E-01 9 3.6788E+00 1.0344E+00 3.3444E-01 1.8725E-01 10 3.0119E+00 9.8700E-01 3.5587E-01 6.8656E-02 12 2.4660E+00 9.2492E-01 3.4538E-01 6.8656E-02 13 2.3653E+00 9.1570E-01 3.3654E-01 6.4672E-02 14 2.3457E+00 9.0468E-01 2.2986E-01 2.1176E-02 16 1.9205E+00 8.0741E-01 2.2810E-01 3.8470E-03 17 1.6530E+00 7.702E-01 1.0148E-01 5.6340E-04 18 1.3534E+00 6.5961E-01 1.0148E-01 5.6340E-05 19 1.0026E+00 5.7702E-01 4.7963E-02 0. 22 6.0810E-01 1.9398E-01 2.1316E-03 0. 23 4.9787E-01 1.3615E-01 2.1316E-03 0. 24 5.683E-01 1.0322E-01 0. 0. 25 2.9721E-01 6.5396E-03 0. 0.	7	6.0653E+00	1.1713E+00	3.3869E-01	2.4085E-01
9 3.6788E+00 1.0344E+00 3.3444E-01 1.8725E-01 10 3.0119E+00 9.8700E-01 3.5268E-01 1.0010E-01 11 2.7253E+00 9.5196E-01 3.5367E-01 6.8656E-02 12 2.4660E+00 9.1270E-01 3.4235E-01 7.2333E-02 13 2.3653E+00 9.1570E-01 3.3654E-01 6.1061E-02 14 2.3457E+00 9.0468E-01 3.2736E-01 2.1176E-02 16 1.9205E+00 8.6739E-01 2.8966E-01 2.1176E-02 16 1.9205E+00 7.4261E-01 1.6934E-01 5.7068E-04 18 1.3534E+00 6.5961E-01 1.0148E-01 5.6340E-05 19 1.0026E+00 5.7702E-01 4.7963E-02 0. 21 7.4274E-01 3.2977E-01 1.4938E-02 0. 22 6.0810E-01 1.9398E-01 6.4499E-03 0. 23 4.9767E-01 1.5017E-04 0. 0. 24 3.6883E-01 1.0322E-01 1.5017E-03 <	8	4.9659E+00	1.1079E+00	3.2516E-01	2.7606E-01
10 3.0119E+00 9.8700E-01 3.5268E-01 1.0010E-01 11 2.7253E+00 9.5196E-01 3.5387E-01 6.8656E-02 12 2.4660E+00 9.2492E-01 3.4283E-01 6.6472E-02 14 2.3457E+00 9.0468E-01 3.2736E-01 6.1061E-02 15 2.2313E+00 8.6739E-01 2.8986E-01 2.1176E-02 16 1.9205E+00 8.0741E-01 2.2810E-01 3.6470E-03 17 1.6530E+00 7.4261E-01 1.0148E-01 5.6340E-05 18 1.3534E+00 6.5961E-01 1.0148E-01 5.6340E-05 19 1.0026E+00 5.7702E-01 4.7963E-02 0. 21 7.4274E-01 3.2977E-01 1.4938E-02 0. 22 6.0810E-01 1.9328E-01 0.1316E-03 0. 23 4.9787E-01 1.3515E-01 2.1316E-03 0. 24 3.6883E-01 1.0322E-01 1.5017E-04 0. 25 2.9721E-01 6.5599E-02 0. 0. 0. 26 1.3316E-01 2.3237E-02 0.	9	3.6788E+00	1.0344E+00	3.3444E-01	1.8725E-01
11 2.7253E+00 9.5196E-01 3.5387E-01 6.8656E-02 12 2.4660E+00 9.2492E-01 3.4283E-01 7.2333E-02 13 2.3653E+00 9.1570E-01 3.3654E-01 6.6472E-02 14 2.3457E+00 9.0468E-01 3.2736E-01 6.1061E-02 15 2.2313E+00 8.6739E-01 2.8986E-01 2.1176E-02 16 1.9205E+00 8.0741E-01 2.2810E-01 3.6470E-03 17 1.6530E+00 7.4261E-01 1.6934E-01 5.7068E-04 18 1.3534E+00 6.5961E-01 1.0148E-01 5.6340E-05 19 1.0026E+00 5.7702E-01 4.7963E-02 0. 20 8.2085E-01 4.9153E-01 2.7746E-02 0. 21 7.4274E-01 3.2977E-01 1.4938E-02 0. 22 6.0810E-01 1.9398E-01 6.4499E-03 0. 23 4.9787E-01 1.5017E-04 0. 0. 24 3.683E-01 1.0322E-01 1.5017E-04 0. 25 2.9721E-01 6.5599E-02 0. 0.	10	3.0119E+00	9.8700E-01	3.5268E-01	1.0010E-01
12 $2.4660E+00$ $9.2492E-01$ $3.4283E-01$ $7.2333E-02$ 13 $2.3653E+00$ $9.1570E-01$ $3.3654E-01$ $6.6472E-02$ 14 $2.3457E+00$ $9.0468E-01$ $3.2736E-01$ $6.1061E-02$ 15 $2.2313E+00$ $8.6739E-01$ $2.8986E-01$ $2.1176E-02$ 16 $1.9205E+00$ $8.6739E-01$ $2.8986E-01$ $3.8470E-03$ 17 $1.6530E+00$ $7.4261E-01$ $1.6934E-01$ $5.7068E-04$ 18 $1.3534E+00$ $6.5961E-01$ $1.0148E-01$ $5.6340E-05$ 19 $1.0026E+00$ $5.7702E-01$ $4.7963E-02$ $0.$ 20 $8.2085E-01$ $4.9153E-01$ $2.7746E-02$ $0.$ 21 $7.4274E-01$ $3.2977E-01$ $1.4938E-02$ $0.$ 22 $6.0610E-01$ $1.9398E-01$ $6.4499E-03$ $0.$ 23 $4.9787E-01$ $1.3615E-01$ $2.1316E-03$ $0.$ 24 $3.6683E-01$ $2.3237E-02$ $0.$ $0.$ 25 $2.9721E-01$ $6.5599E-02$ $0.$ $0.$ 26 $1.8316E-01$ $2.3237E-02$ $0.$ $0.$ 29 $4.0868E-02$ $3.5663E-06$ $0.$ $0.$ 30 $3.1828E-02$ $0.$ $0.$ $0.$ 31 $2.6058E-02$ $0.$ $0.$ $0.$ 32 $2.1476E-02$ $0.$ $0.$ $0.$ 33 $2.1875E-02$ $0.$ $0.$ $0.$ 34 $1.5034E-02$ $0.$ $0.$ $0.$ 35 $7.1017E-03$ $0.$ $0.$ $0.$ </td <td>11</td> <td>2.7253E+00</td> <td>9.5196E-01</td> <td>3.5387E-01</td> <td>6.8656E-02</td>	11	2.7253E+00	9.5196E-01	3.5387E-01	6.8656E-02
13 2.3653E+00 9.1570E-01 3.3654E-01 6.6472E-02 14 2.3457E+00 8.6739E-01 2.8986E-01 2.1176E-02 16 1.9205E+00 8.0741E-01 2.2810E-01 3.8470E-03 17 1.6530E+00 7.4261E-01 1.6934E-01 5.7068E-04 18 1.3534E+00 6.5961E-01 1.0148E-01 5.6340E-05 19 1.026E+00 5.7702E-01 4.7963E-02 0. 21 7.4274E-01 3.2977E-01 1.4938E-02 0. 22 6.0810E-01 1.9398E-01 6.4499E-03 0. 23 4.9787E-01 1.3615E-01 2.1316E-03 0. 24 3.6883E-01 1.0322E-01 1.5017E-04 0. 25 2.9721E-01 6.5599E-02 0. 0. 0. 26 1.8316E-01 2.3237E-02 0. 0. 0. 29 4.0868E-02 3.5663E-06 0. 0. 0. 31 2.6058E-02 0. 0. 0. 0. 32 2.4176E-02 0. 0. 0.	12	2.4660E+00	9.2492E-01	3.4283E-01	7.2333E-02
14 2.3457E+00 9.0468E-01 3.2736E-01 6.1061E-02 15 2.2313E+00 8.6739E-01 2.8986E-01 2.1176E-02 16 1.9205E+00 8.0741E-01 2.2810E-01 3.8470E-03 17 1.6530E+00 7.4261E-01 1.6934E-01 5.7068E-04 18 1.3534E+00 6.5961E-01 1.0148E-01 5.6340E-05 19 1.0026E+00 5.7702E-01 4.7963E-02 0. 20 8.2085E-01 4.9153E-01 2.7746E-02 0. 21 7.4274E-01 3.2977E-01 1.4938E-02 0. 22 6.0810E-01 1.9398E-01 6.4499E-03 0. 23 4.9787E-01 1.3615E-01 2.1316E-03 0. 24 3.6883E-01 1.0322E-01 1.5017E-04 0. 25 2.9721E-01 6.5599E-02 0. 0. 0. 26 1.8316E-01 2.3237E-02 0. 0. 0. 28 6.7379E-02 1.63560E-03 0. 0. 0. 30 3.1828E-02 0. 0. 0.	13	2.3653E+00	9.1570E-01	3.3654E-01	6.6472E-02
15 $2.2313E+00$ $8.6739E-01$ $2.8966E-01$ $2.1176E-02$ 16 $1.9205E+00$ $8.0741E-01$ $2.2810E-01$ $3.8470E-03$ 17 $1.6530E+00$ $7.4261E-01$ $1.6934E-01$ $5.7068E-04$ 18 $1.3534E+00$ $6.5961E-01$ $1.0148E-01$ $5.6340E-05$ 19 $1.0026E+00$ $5.7702E-01$ $4.7963E-02$ $0.$ 20 $8.2085E-01$ $4.9153E-01$ $2.7746E-02$ $0.$ 21 $7.4274E-01$ $3.2977E-01$ $1.4938E-02$ $0.$ 22 $6.0810E-01$ $1.9398E-01$ $6.4499E-03$ $0.$ 23 $4.9787E-01$ $1.3615E-01$ $2.1316E-03$ $0.$ 24 $3.6883E-01$ $1.0322E-01$ $1.5017E-04$ $0.$ 25 $2.9721E-01$ $6.5599E-02$ $0.$ $0.$ 26 $1.8316E-01$ $2.3237E-02$ $0.$ $0.$ 27 $1.1109E-01$ $5.3946E-03$ $0.$ $0.$ 28 $6.7379E-02$ $0.$ $0.$ $0.$ 30 $3.1828E-02$ $0.$ $0.$ $0.$ 31 $2.6058E-02$ $0.$ $0.$ $0.$ 32 $2.4176E-02$ $0.$ $0.$ $0.$ 33 $2.1875E-02$ $0.$ $0.$ $0.$ 34 $1.5034E-03$ $0.$ $0.$ $0.$ 35 $7.1017E-03$ $0.$ $0.$ $0.$ 36 $3.546E-03$ $0.$ $0.$ $0.$ 37 $1.5846E-03$ $0.$ $0.$ $0.$ 38 $4.5400E-04$ $0.$ $0.$	14	2.3457E+00	9.0468E-01	3.2736E-01	6.1061E-02
16 $1.9205E+00$ $8.0741E-01$ $2.2810E-01$ $3.8470E-03$ 17 $1.6530E+00$ $7.4261E-01$ $1.6934E-01$ $5.7068E-04$ 18 $1.3534E+00$ $6.5961E-01$ $1.0148E-01$ $5.6340E-05$ 19 $1.0026E+00$ $5.7702E-01$ $4.7963E-02$ $1.2101E-06$ 20 $8.2085E-01$ $4.9153E-01$ $2.7746E-02$ $0.$ 21 $7.4274E-01$ $3.2977E-01$ $1.4938E-02$ $0.$ 22 $6.0810E-01$ $1.9398E-01$ $6.4499E-03$ $0.$ 23 $4.9787E-01$ $1.3615E-01$ $2.1316E-03$ $0.$ 24 $3.6883E-01$ $1.0322E-01$ $1.5017E-04$ $0.$ 25 $2.9721E-01$ $6.5599E-02$ $0.$ $0.$ 26 $1.8316E-01$ $2.3237E-02$ $0.$ $0.$ 27 $1.1109E-01$ $5.3946E-03$ $0.$ $0.$ 28 $6.7379E-02$ $1.6350E-03$ $0.$ $0.$ 29 $4.0868E-02$ $0.$ $0.$ $0.$ 31 $2.6058E-02$ $0.$ $0.$ $0.$ 32 $2.4176E-02$ $0.$ $0.$ $0.$ 33 $2.1875E-02$ $0.$ $0.$ $0.$ 34 $1.5034E-03$ $0.$ $0.$ $0.$ 35 $7.1017E-03$ $0.$ $0.$ $0.$ 36 $3.3546E-03$ $0.$ $0.$ $0.$ 39 $2.1445E-04$ $0.$ $0.$ $0.$ 39 $2.1445E-04$ $0.$ $0.$ $0.$ 40 $1.0130E-04$ $0.$ $0.$ $0.$	15	2.2313E+00	8.6739E-01	2.8986E-01	2.1176E-02
17 1.6530E+00 7.4261E-01 1.6934E-01 5.7068E-04 18 1.3534E+00 6.5961E-01 1.0148E-01 5.6340E-05 19 1.0026E+00 5.7702E-01 4.7963E-02 1.2101E-06 20 8.2085E-01 4.9153E-01 2.7746E-02 0. 21 7.4274E-01 3.2977E-01 1.4938E-02 0. 22 6.0810E-01 1.3938E-01 6.4499E-03 0. 23 4.9787E-01 1.3615E-01 2.1316E-03 0. 24 3.6883E-01 1.0322E-01 1.5017E-04 0. 25 2.9721E-01 6.5599E-02 0. 0. 0. 26 1.8316E-01 2.3237E-02 0. 0. 0. 27 1.1109E-01 5.3946E-03 0. 0. 0. 28 6.7379E-02 1.6350E-03 0. 0. 0. 30 3.1828E-02 0. 0. 0. 0. 31 2.6058E-02 0. 0. 0. 0. 32 2.4176E-02 0. 0. 0. <td>16</td> <td>1.9205E+00</td> <td>8.0741E-01</td> <td>2.2810E-01</td> <td>3.8470E-03</td>	16	1.9205E+00	8.0741E-01	2.2810E-01	3.8470E-03
18 1.3534E+00 6.5961E-01 1.0148E-01 5.6340E-05 19 1.0026E+00 5.7702E-01 4.7963E-02 1.2101E-06 20 8.2085E-01 4.9153E-01 2.7746E-02 0. 21 7.4274E-01 3.2977E-01 1.4938E-02 0. 22 6.0810E-01 1.9398E-01 6.4499E-03 0. 23 4.9787E-01 1.3615E-01 2.1316E-03 0. 24 3.6883E-01 1.0322E-01 1.5017E-04 0. 25 2.9721E-01 6.5599E-02 0. 0. 0. 26 1.8316E-01 2.3237E-02 0. 0. 0. 27 1.109F-01 5.3946E-03 0. 0. 0. 28 6.7379E-02 1.6350E-03 0. 0. 0. 31 2.6058E-02 0. 0. 0. 0. 32 2.4176E-02 0. 0. 0. 0. 33 2.1875E-02 0. 0. 0. 0. 34 1.5034E-03 0. 0. 0.	17	1.6530E+00	7.4261E-01	1.6934E-01	5.7068E-04
19 1.0026E+00 5.7702E-01 4.7963E-02 1.2101E-06 20 8.2085E-01 4.9153E-01 2.7746E-02 0. 21 7.4274E-01 3.2977E-01 1.4938E-02 0. 22 6.0810E-01 1.9398E-01 6.4499E-03 0. 23 4.9787E-01 1.3615E-01 2.1316E-03 0. 24 3.6883E-01 1.0322E-01 1.5017E-04 0. 25 2.9721E-01 6.55998E-02 0. 0. 26 1.8316E-01 2.3237E-02 0. 0. 27 1.1109E-01 5.3946E-03 0. 0. 28 6.7379E-02 1.6350E-03 0. 0. 30 3.1828E-02 0. 0. 0. 31 2.6058E-02 0. 0. 0. 33 2.1875E-02 0. 0. 0. 33 2.1875E-02 0. 0. 0. 33 2.1875E-02 0. 0. 0. 34 1.5034E-03 0. 0. 0. 35 <td>18</td> <td>1.3534E+00</td> <td>6.5961E-01</td> <td>1.0148E-01</td> <td>5.6340E-05</td>	18	1.3534E+00	6.5961E-01	1.0148E-01	5.6340E-05
20 8.2085E-01 4.9153E-01 2.7746E-02 0. 21 7.4274E-01 3.2977E-01 1.4938E-02 0. 22 6.0810E-01 1.9398E-01 6.4499E-03 0. 23 4.9787E-01 1.3615E-01 2.1316E-03 0. 24 3.6883E-01 1.0322E-01 1.5017E-04 0. 25 2.9721E-01 6.5599E-02 0. 0. 26 1.8316E-01 2.3237E-02 0. 0. 27 1.1109E-01 5.3946E-03 0. 0. 28 6.7379E-02 1.6350E-03 0. 0. 30 3.1828E-02 0. 0. 0. 31 2.6058E-02 0. 0. 0. 33 2.1875E-02 0. 0. 0. 34 1.5034E-02 0. 0. 0. 35 7.1017E-03 0. 0. 0. 36 3.3546E-03 0. 0. 0. 37 1.5846E-03 0. 0. 0. 38 4.5400E-04 <td>19</td> <td>1.0026E+00</td> <td>5.7702E-01</td> <td>4.7963E-02</td> <td>1.2101E-06</td>	19	1.0026E+00	5.7702E-01	4.7963E-02	1.2101E-06
21 $7.4274E-01$ $3.2977E-01$ $1.4938E-02$ $0.$ 22 $6.0810E-01$ $1.9398E-01$ $6.4499E-03$ $0.$ 23 $4.9787E-01$ $1.3615E-01$ $2.1316E-03$ $0.$ 24 $3.6883E-01$ $1.0322E-01$ $1.5017E-04$ $0.$ 25 $2.9721E-01$ $6.5599E-02$ $0.$ $0.$ 26 $1.8316E-01$ $2.3237E-02$ $0.$ $0.$ 27 $1.109E-01$ $5.3946E-03$ $0.$ $0.$ 28 $6.7379E-02$ $1.6350E-03$ $0.$ $0.$ 29 $4.0868E-02$ $3.5663E-06$ $0.$ $0.$ 30 $3.1828E-02$ $0.$ $0.$ $0.$ 31 $2.6058E-02$ $0.$ $0.$ $0.$ 32 $2.4176E-02$ $0.$ $0.$ $0.$ 33 $2.1875E-02$ $0.$ $0.$ $0.$ 34 $1.5034E-03$ $0.$ $0.$ $0.$ 35 $7.1017E-03$ $0.$ $0.$ $0.$ 36 $3.3546E-03$ $0.$ $0.$ $0.$ 39 $2.1445E-04$ $0.$ $0.$ $0.$ 40 $1.0130E-04$ $0.$ $0.$ $0.$ 41 $3.7266E-05$ $0.$ $0.$ $0.$ 43 $5.0435E-06$ $0.$ $0.$ $0.$ 44 $1.8554E-06$ $0.$ $0.$ $0.$ 45 $8.7643E-07$ $0.$ $0.$ $0.$ 47 $1.0000E-07$ $0.$ $0.$ $0.$	20	8.2085E-01	4.9153E-01	2.7746E-02	0.
22 6.0810E-01 1.93988-01 6.4499E-03 0. 23 4.9787E-01 1.3615E-01 2.1316E-03 0. 24 3.6883E-01 1.0322E-01 1.5017E-04 0. 25 2.9721E-01 6.5599E-02 0. 0. 26 1.8316E-01 2.3237E-02 0. 0. 27 1.1109E-01 5.3946E-03 0. 0. 28 6.7379E-02 1.6350E-03 0. 0. 29 4.0868E-02 3.5663E-06 0. 0. 30 3.1828E-02 0. 0. 0. 31 2.6058E-02 0. 0. 0. 33 2.1875E-02 0. 0. 0. 34 1.5034E-02 0. 0. 0. 35 7.1017E-03 0. 0. 0. 38 4.5400E-04 0. 0. 0. 39 2.1445E-04 0. 0. 0. 40 1.0130E-04 0. 0. 0. 42 1.0677E-05 0.	21	7.4274E-01	3.2977E-01	1.4938E-02	0.
23 4.9787E-01 1.3615E-01 2.1316E-03 0. 24 3.6883E-01 1.0322E-01 1.5017E-04 0. 25 2.9721E-01 6.5599E-02 0. 0. 26 1.8316E-01 2.3237E-02 0. 0. 27 1.1109E-01 5.3946E-03 0. 0. 28 6.7379E-02 1.6350E-03 0. 0. 29 4.0868E-02 3.5663E-06 0. 0. 30 3.1828E-02 0. 0. 0. 31 2.6058E-02 0. 0. 0. 33 2.1875E-02 0. 0. 0. 34 1.5034E-02 0. 0. 0. 34 1.5034E-02 0. 0. 0. 35 7.1017E-03 0. 0. 0. 36 3.3546E-03 0. 0. 0. 38 4.5400E-04 0. 0. 0. 39 2.1445E-04 0. 0. 0. 41 3.7266E-05 0. 0.	22	6.0810E-01	1.9398E-01	6.4499E-03	0.
24 3.6883E-01 1.0322E-01 1.5017E-04 0. 25 2.9721E-01 6.5599E-02 0. 0. 26 1.8316E-01 2.3237E-02 0. 0. 27 1.1109E-01 5.3946E-03 0. 0. 28 6.7379E-02 1.6350E-03 0. 0. 29 4.0868E-02 3.5663E-06 0. 0. 30 3.1828E-02 0. 0. 0. 32 2.4176E-02 0. 0. 0. 33 2.1875E-02 0. 0. 0. 34 1.5034E-03 0. 0. 0. 34 1.5034E-03 0. 0. 0. 35 7.1017E-03 0. 0. 0. 36 3.3546E-03 0. 0. 0. 39 2.1445E-04 0. 0. 0. 39 2.1445E-04 0. 0. 0. 41 3.7266E-05 0. 0. 0. 42 1.0677E-05 0. 0. 0.	23	4.9787E-01	1.3615E-01	2.1316E-03	0.
25 $2.9721E-01$ $6.5599E-02$ $0.$ $0.$ 26 $1.8316E-01$ $2.3237E-02$ $0.$ $0.$ 27 $1.1109E-01$ $5.3946E-03$ $0.$ $0.$ 28 $6.7379E-02$ $1.6350E-03$ $0.$ $0.$ 29 $4.0868E-02$ $3.5663E-06$ $0.$ $0.$ 30 $3.1828E-02$ $0.$ $0.$ $0.$ 31 $2.6058E-02$ $0.$ $0.$ $0.$ 32 $2.4176E-02$ $0.$ $0.$ $0.$ 33 $2.1875E-02$ $0.$ $0.$ $0.$ 34 $1.5034E-02$ $0.$ $0.$ $0.$ 34 $1.5034E-02$ $0.$ $0.$ $0.$ 35 $7.1017E-03$ $0.$ $0.$ $0.$ 36 $3.3546E-03$ $0.$ $0.$ $0.$ 37 $1.5846E-03$ $0.$ $0.$ $0.$ 38 $4.5400E-04$ $0.$ $0.$ $0.$ 40 $1.0130E-04$ $0.$ $0.$ $0.$ 41 $3.7266E-05$ $0.$ $0.$ $0.$ 42 $1.0677E-05$ $0.$ $0.$ $0.$ 43 $5.0435E-06$ $0.$ $0.$ $0.$ 44 $1.8554E-06$ $0.$ $0.$ $0.$ 44 $1.8554E-06$ $0.$ $0.$ $0.$ 45 $8.7643E-07$ $0.$ $0.$ $0.$ 47 $1.0000E-07$ $0.$ $0.$ $0.$	24	3.6883E-01	1.0322E-01	1.5017E-04	0.
26 $1.8316E-01$ $2.3237E-02$ $0.$ $0.$ 27 $1.1109E-01$ $5.3946E-03$ $0.$ $0.$ 28 $6.7379E-02$ $1.6350E-03$ $0.$ $0.$ 29 $4.0868E-02$ $3.5663E-06$ $0.$ $0.$ 30 $3.1828E-02$ $0.$ $0.$ $0.$ 31 $2.6058E-02$ $0.$ $0.$ $0.$ 32 $2.4176E-02$ $0.$ $0.$ $0.$ 33 $2.1875E-02$ $0.$ $0.$ $0.$ 34 $1.5034E-02$ $0.$ $0.$ $0.$ 35 $7.1017E-03$ $0.$ $0.$ $0.$ 36 $3.3546E-03$ $0.$ $0.$ $0.$ 37 $1.5846E-03$ $0.$ $0.$ $0.$ 38 $4.5400E-04$ $0.$ $0.$ $0.$ 40 $1.0130E-04$ $0.$ $0.$ $0.$ 41 $3.7266E-05$ $0.$ $0.$ $0.$ 42 $1.0677E-05$ $0.$ $0.$ $0.$ 43 $5.0435E-06$ $0.$ $0.$ $0.$ 44 $1.8554E-06$ $0.$ $0.$ $0.$ 45 $8.7643E-07$ $0.$ $0.$ $0.$ 46 $4.1399E-07$ $0.$ $0.$ $0.$ 47 $1.0000E-011$ $0.$ $0.$ $0.$	25	2.9721E-01	6.5599E-02	0.	0.
271.1109E-01 $5.3946E-03$ 0.0. 28 $6.7379E-02$ $1.6350E-03$ 0.0. 29 $4.0868E-02$ $3.5663E-06$ 0.0. 30 $3.1828E-02$ 0.0.0. 31 $2.6058E-02$ 0.0.0. 32 $2.4176E-02$ 0.0.0. 33 $2.1875E-02$ 0.0.0. 34 $1.5034E-02$ 0.0.0. 34 $1.5034E-02$ 0.0.0. 35 $7.1017E-03$ 0.0.0. 36 $3.3546E-03$ 0.0.0. 37 $1.5846E-03$ 0.0.0. 38 $4.5400E-04$ 0.0.0. 39 $2.1445E-04$ 0.0.0. 40 $1.0130E-04$ 0.0.0. 41 $3.7266E-05$ 0.0.0. 42 $1.0677E-05$ 0.0.0. 43 $5.0435E-06$ 0.0.0. 44 $1.8554E-06$ 0.0.0. 45 $8.7643E-07$ 0.0.0. 46 $4.1399E-07$ 0.0.0. 47 $1.0000E-07$ 0.0.0. $1.0000E-11$ $0.$ $0.$ $0.$ $0.$	26	1.8316E-01	2.3237E-02	0.	0.
28 $6.7379E-02$ $1.6350E-03$ $0.$ $0.$ 29 $4.0868E-02$ $3.5663E-06$ $0.$ $0.$ 30 $3.1828E-02$ $0.$ $0.$ $0.$ 31 $2.6058E-02$ $0.$ $0.$ $0.$ 32 $2.4176E-02$ $0.$ $0.$ $0.$ 33 $2.1875E-02$ $0.$ $0.$ $0.$ 34 $1.5034E-02$ $0.$ $0.$ $0.$ 35 $7.1017E-03$ $0.$ $0.$ $0.$ 36 $3.3546E-03$ $0.$ $0.$ $0.$ 37 $1.5846E-03$ $0.$ $0.$ $0.$ 38 $4.5400E-04$ $0.$ $0.$ $0.$ 40 $1.0130E-04$ $0.$ $0.$ $0.$ 41 $3.7266E-05$ $0.$ $0.$ $0.$ 43 $5.0435E-06$ $0.$ $0.$ $0.$ 44 $1.8554E-06$ $0.$ $0.$ $0.$ 44 $1.8554E-06$ $0.$ $0.$ $0.$ 46 $4.1399E-07$ $0.$ $0.$ $0.$ 47 $1.0000E-07$ $0.$ $0.$ $0.$	27	1.1109E-01	5.3946E-03	0.	0.
29 $4.0868E-02$ $3.5663E-06$ $0.$ $0.$ 30 $3.1828E-02$ $0.$ $0.$ $0.$ 31 $2.6058E-02$ $0.$ $0.$ $0.$ 32 $2.4176E-02$ $0.$ $0.$ $0.$ 33 $2.1875E-02$ $0.$ $0.$ $0.$ 34 $1.5034E-02$ $0.$ $0.$ $0.$ 35 $7.1017E-03$ $0.$ $0.$ $0.$ 36 $3.3546E-03$ $0.$ $0.$ $0.$ 37 $1.5846E-03$ $0.$ $0.$ $0.$ 38 $4.5400E-04$ $0.$ $0.$ $0.$ 39 $2.1445E-04$ $0.$ $0.$ $0.$ 40 $1.0130E-04$ $0.$ $0.$ $0.$ 41 $3.7266E-05$ $0.$ $0.$ $0.$ 42 $1.0677E-05$ $0.$ $0.$ $0.$ 43 $5.0435E-06$ $0.$ $0.$ $0.$ 44 $1.8554E-06$ $0.$ $0.$ $0.$ 45 $8.7643E-07$ $0.$ $0.$ $0.$ 46 $4.1399E-07$ $0.$ $0.$ $0.$ 47 $1.0000E-07$ $0.$ $0.$ $0.$	28	6.7379E-02	1.6350E-03	0.	0.
30 $3.1828E-02$ $0.$ $0.$ $0.$ $0.$ 31 $2.6058E-02$ $0.$ $0.$ $0.$ $0.$ 32 $2.4176E-02$ $0.$ $0.$ $0.$ $0.$ 33 $2.1875E-02$ $0.$ $0.$ $0.$ $0.$ 34 $1.5034E-02$ $0.$ $0.$ $0.$ $0.$ 35 $7.1017E-03$ $0.$ $0.$ $0.$ $0.$ 36 $3.3546E-03$ $0.$ $0.$ $0.$ $0.$ 37 $1.5846E-03$ $0.$ $0.$ $0.$ $0.$ 38 $4.5400E-04$ $0.$ $0.$ $0.$ $0.$ 40 $1.0130E-04$ $0.$ $0.$ $0.$ $0.$ 41 $3.7266E-05$ $0.$ $0.$ $0.$ $0.$ 43 $5.0435E-06$ $0.$ $0.$ $0.$ $0.$ 44 $1.8554E-06$ $0.$ $0.$ $0.$ $0.$ 45 $8.7643E-07$ $0.$ $0.$ $0.$ $0.$ 46 $4.1399E-07$ $0.$ $0.$ $0.$ $0.$ 47 $1.0000E-07$ $0.$ $0.$ $0.$ $0.$	29	4.0868E-02	3.5663E-06	0.	0.
312.6058E-020.0.0.0. 32 2.4176E-020.0.0.0. 33 2.1875E-020.0.0.0. 34 1.5034E-020.0.0.0. 35 7.1017E-030.0.0.0. 36 3.3546E-030.0.0.0. 37 1.5846E-030.0.0.0. 38 4.5400E-040.0.0.0. 39 2.1445E-040.0.0.0. 40 1.0130E-040.0.0.0. 41 3.7266E-050.0.0.0. 42 1.0677E-050.0.0.0. 43 5.0435E-060.0.0.0. 44 1.8554E-060.0.0.0. 45 8.7643E-070.0.0.0. 46 4.1399E-070.0.0.0. 47 1.0000E-070.0.0.0.	30	3.1828E-02	0.	0.	0.
32 $2.4176E-02$ $0.$ $0.$ $0.$ $0.$ 33 $2.1875E-02$ $0.$ $0.$ $0.$ $0.$ 34 $1.5034E-02$ $0.$ $0.$ $0.$ $0.$ 35 $7.1017E-03$ $0.$ $0.$ $0.$ 36 $3.3546E-03$ $0.$ $0.$ $0.$ 37 $1.5846E-03$ $0.$ $0.$ $0.$ 38 $4.5400E-04$ $0.$ $0.$ $0.$ 39 $2.1445E-04$ $0.$ $0.$ $0.$ 40 $1.0130E-04$ $0.$ $0.$ $0.$ 41 $3.7266E-05$ $0.$ $0.$ $0.$ 42 $1.0677E-05$ $0.$ $0.$ $0.$ 43 $5.0435E-06$ $0.$ $0.$ $0.$ 44 $1.8554E-06$ $0.$ $0.$ $0.$ 45 $8.7643E-07$ $0.$ $0.$ $0.$ 46 $4.1399E-07$ $0.$ $0.$ $0.$ 47 $1.0000E-07$ $0.$ $0.$ $0.$	31	2.6058E-02	0.	0.	0.
33 $2.1875E-02$ $0.$ $0.$ $0.$ $0.$ 34 $1.5034E-02$ $0.$ $0.$ $0.$ $0.$ 35 $7.1017E-03$ $0.$ $0.$ $0.$ $0.$ 36 $3.3546E-03$ $0.$ $0.$ $0.$ $0.$ 37 $1.5846E-03$ $0.$ $0.$ $0.$ $0.$ 38 $4.5400E-04$ $0.$ $0.$ $0.$ $0.$ 39 $2.1445E-04$ $0.$ $0.$ $0.$ $0.$ 40 $1.0130E-04$ $0.$ $0.$ $0.$ $0.$ 41 $3.7266E-05$ $0.$ $0.$ $0.$ $0.$ 42 $1.0677E-05$ $0.$ $0.$ $0.$ $0.$ 43 $5.0435E-06$ $0.$ $0.$ $0.$ $0.$ 44 $1.8554E-06$ $0.$ $0.$ $0.$ $0.$ 45 $8.7643E-07$ $0.$ $0.$ $0.$ $0.$ 46 $4.1399E-07$ $0.$ $0.$ $0.$ $0.$ 47 $1.0000E-07$ $0.$ $0.$ $0.$ $0.$	32	2.41/6E-02	0.	0.	0.
341.5034E-020.0.0.0. 35 7.1017E-030.0.0.0. 36 3.3546E-030.0.0.0. 37 1.5846E-030.0.0.0. 38 4.5400E-040.0.0.0. 39 2.1445E-040.0.0.0. 40 1.0130E-040.0.0.0. 41 3.7266E-050.0.0.0. 42 1.0677E-050.0.0.0. 43 5.0435E-060.0.0.0. 44 1.8554E-060.0.0.0. 45 8.7643E-070.0.0.0. 46 4.1399E-070.0.0.0. 47 1.0000E-070.0.0.0. $1.0000E-111$ 0.0.0.0.	33	2.18/5E-02	0.	0.	0.
35 $7.1017E-03$ 0.0.0.36 $3.3546E-03$ 0.0.0.37 $1.5846E-03$ 0.0.0.38 $4.5400E-04$ 0.0.0.39 $2.1445E-04$ 0.0.0.40 $1.0130E-04$ 0.0.0.41 $3.7266E-05$ 0.0.0.42 $1.0677E-05$ 0.0.0.43 $5.0435E-06$ 0.0.0.44 $1.8554E-06$ 0.0.0.45 $8.7643E-07$ 0.0.0.46 $4.1399E-07$ 0.0.0.47 $1.0000E-07$ 0.0.0. $1.0000E-11$ $0.$ $0.$ $0.$	34	1.5034E-02	0.	0.	0.
36 $3.3346E-03$ $0.$ $0.$ $0.$ $0.$ 37 $1.5846E-03$ $0.$ $0.$ $0.$ 38 $4.5400E-04$ $0.$ $0.$ $0.$ 39 $2.1445E-04$ $0.$ $0.$ $0.$ 40 $1.0130E-04$ $0.$ $0.$ $0.$ 41 $3.7266E-05$ $0.$ $0.$ $0.$ 42 $1.0677E-05$ $0.$ $0.$ $0.$ 43 $5.0435E-06$ $0.$ $0.$ $0.$ 44 $1.8554E-06$ $0.$ $0.$ $0.$ 45 $8.7643E-07$ $0.$ $0.$ $0.$ 46 $4.1399E-07$ $0.$ $0.$ $0.$ 47 $1.0000E-07$ $0.$ $0.$ $0.$ $1.0000E-11$ $0.$ $0.$ $0.$	35	7.101/E-03	0.	0.	0.
37 $1.3848E-03$ $0.$ $0.$ $0.$ $0.$ 38 $4.5400E-04$ $0.$ $0.$ $0.$ $0.$ 39 $2.1445E-04$ $0.$ $0.$ $0.$ 40 $1.0130E-04$ $0.$ $0.$ $0.$ 41 $3.7266E-05$ $0.$ $0.$ $0.$ 42 $1.0677E-05$ $0.$ $0.$ $0.$ 43 $5.0435E-06$ $0.$ $0.$ $0.$ 44 $1.8554E-06$ $0.$ $0.$ $0.$ 45 $8.7643E-07$ $0.$ $0.$ $0.$ 46 $4.1399E-07$ $0.$ $0.$ $0.$ 47 $1.0000E-07$ $0.$ $0.$ $0.$ $1.0000E-11$ $0.$ $0.$ $0.$	30	3.3540E-03 1 5946E-03	0.	0.	0.
36 $4.3400E-04$ $0.$ $0.$ $0.$ $0.$ 39 $2.1445E-04$ $0.$ $0.$ $0.$ $0.$ 40 $1.0130E-04$ $0.$ $0.$ $0.$ 41 $3.7266E-05$ $0.$ $0.$ $0.$ 42 $1.0677E-05$ $0.$ $0.$ $0.$ 43 $5.0435E-06$ $0.$ $0.$ $0.$ 44 $1.8554E-06$ $0.$ $0.$ $0.$ 45 $8.7643E-07$ $0.$ $0.$ $0.$ 46 $4.1399E-07$ $0.$ $0.$ $0.$ 47 $1.0000E-07$ $0.$ $0.$ $0.$ $1.0000E-11$ $0.$ $0.$ $0.$	37	1.5840E-03	0.	0.	0.
39 2.1445E 04 0. 0. 0. 40 1.0130E-04 0. 0. 0. 41 3.7266E-05 0. 0. 0. 42 1.0677E-05 0. 0. 0. 43 5.0435E-06 0. 0. 0. 44 1.8554E-06 0. 0. 0. 45 8.7643E-07 0. 0. 0. 46 4.1399E-07 0. 0. 0. 47 1.0000E-07 0. 0. 0 1.0000E-11 0 0. 0. 0	30	4.3400E-04 2 1445F-04	0.	0.	0.
40 1.0130E 04 0. 0. 0. 41 3.7266E-05 0. 0. 0. 42 1.0677E-05 0. 0. 0. 43 5.0435E-06 0. 0. 0. 44 1.8554E-06 0. 0. 0. 45 8.7643E-07 0. 0. 0. 46 4.1399E-07 0. 0. 0. 47 1.0000E-07 0. 0. 0 1.0000E-11 0 0. 0 0	39	1 0130F - 04	0.	0	0.
41 5.72001 05 0. 0. 0. 42 1.0677E-05 0. 0. 0. 43 5.0435E-06 0. 0. 0. 44 1.8554E-06 0. 0. 0. 45 8.7643E-07 0. 0. 0. 46 4.1399E-07 0. 0. 0. 47 1.0000E-07 0. 0. 0 1.0000E-11 0. 0. 0 0	40	3 7266E-05	0.	0	0.
43 5.0435E-06 0. 0. 0. 0. 44 1.8554E-06 0. 0. 0. 0. 45 8.7643E-07 0. 0. 0. 0. 46 4.1399E-07 0. 0. 0. 0. 47 1.0000E-07 0. 0. 0. 0. 1.0000E-11 0. 0. 0. 0. 0.	42	1.0677E-05	0	0	0.
44 1.8554E-06 0. 0. 0. 0. 45 8.7643E-07 0. 0. 0. 0. 46 4.1399E-07 0. 0. 0. 0. 47 1.0000E-07 0. 0. 0. 0. 1.0000E-11 0. 0. 0. 0.	42	5.0435E-06	0	0	0
45 8.7643E-07 0. 0. 0. 46 4.1399E-07 0. 0. 0. 47 1.0000E-07 0. 0. 0 1.0000E-11 0. 0. 0 0	45	1.8554E-06	0	<u> </u>	0
46 4.1399E-07 0. 0. 0. 47 1.0000E-07 0. 0. 0 1.0000E-11 0. 0. 0	45	8.7643E-07	0.	0.	0.
47 1.0000E-07 0. 0. 0 1.0000E-11	46	4.1399E-07	0.	0.	0.
1.000E-11	47	1.0000E-07	0.	0.	0
		1.0000E-11	-		



IRDF-2002 1/4 T RPV Weighting Neutron Dosimeter Cross Sections [barns] Used in the TORT-3.2 Calculations with the BUGENDF70.BOLIB Library.

6	Upper Energy	Rh-103	In-115	S-32
Group	[MeV]	(n,n')	(n,n')	(n,p)
1	1.7332E+01	2.4736E-01	5.9174E-02	1.9504E-01
2	1.4191E+01	4.0943E-01	9.8495E-02	3.1939E-01
3	1.2214E+01	8.8628E-01	2.1529E-01	3.7877E-01
4	1.0000E+01	1.2280E+00	2.7602E-01	3.3756E-01
5	8.6071E+00	1.2743E+00	3.1014E-01	3.2279E-01
6	7.4082E+00	1.2259E+00	3.3553E-01	3.1134E-01
7	6.0653E+00	1.1713E+00	3.3870E-01	2.4087E-01
8	4.9659E+00	1.1080E+00	3.2519E-01	2.7597E-01
9	3.6788E+00	1.0340E+00	3.3463E-01	1.8679E-01
10	3.0119E+00	9.8681E-01	3.5274E-01	9.9856E-02
11	2.7253E+00	9.5184E-01	3.5384E-01	6.8690E-02
12	2.4660E+00	9.2505E-01	3.4291E-01	7.2357E-02
13	2.3653E+00	9.1570E-01	3.3654E-01	6.6472E-02
14	2.3457E+00	9.0476E-01	3.2744E-01	6.1120E-02
15	2.2313E+00	8.6750E-01	2.8997E-01	2.1288E-02
16	1.9205E+00	8.0709E-01	2.2780E-01	3.8128E-03
17	1.6530E+00	7.4285E-01	1.6955E-01	5.7288E-04
18	1.3534E+00	6.5898E-01	1.0098E-01	5.5136E-05
19	1.0026E+00	5.7853E-01	4.8555E-02	1.3091E-06
20	8.2085E-01	4.9180E-01	2.7780E-02	0.
21	7.4274E-01	3.2413E-01	1.4595E-02	0.
22	6.0810E-01	1.9458E-01	6.4916E-03	0.
23	4.9787E-01	1.3637E-01	2.1464E-03	0.
24	3.6883E-01	1.0321E-01	1.5024E-04	0.
25	2.9721E-01	6.5947E-02	0.	0.
26	1.8316E-01	2.3120E-02	0.	0.
27	1.1109E-01	5.3290E-03	0.	0.
28	6.7379E-02	1.6314E-03	0.	0.
29	4.0868E-02	3.5772E-06	0.	0.
30	3.1828E-02	0.	0.	0.
31	2.6058E-02	0.	0.	0.
32	2.4176E-02	0.	0.	0.
33	2.1875E-02	0.	0.	0.
34	1.5034E-02	0.	0.	0.
35	7.1017E-03	0.	0.	0.
36	3.3546E-03	0.	0.	0.
37	1.5846E-03	0.	0.	0.
38	4.5400E-04	0.	0.	0.
39	2.1445E-04	0.	0.	0.
40	1.0130E-04	0.	0.	0.
41	3.7266E-05	0.	0.	0.
42	1.0677E-05	0.	0.	0.
43	5.0435E-06	0.	0.	0.
44	1.8554E-06	0.	0.	0.
45	8.7643E-07	0.	0.	0.
46	4.1399E-07	0.	0.	0.
47	1.0000E-07	0.	0.	0.
	1.0000E-11			



IRDF-2002 1/4 T RPV Weighting Neutron Dosimeter Cross Sections [barns] Used in the TORT-3.2 Calculations with the BUGLE-96 Library.

0	Upper Energy	Rh-103	In-115	S-32
Group	[MeV]	(n,n')	(n,n')	(n,p)
1	1.7332E+01	2.4772E-01	5.9202E-02	1.9559E-01
2	1.4191E+01	4.0865E-01	9.8250E-02	3.1902E-01
3	1.2214E+01	8.8555E-01	2.1510E-01	3.7870E-01
4	1.0000E+01	1.2278E+00	2.7598E-01	3.3761E-01
5	8.6071E+00	1.2744E+00	3.1003E-01	3.2271E-01
6	7.4082E+00	1.2258E+00	3.3556E-01	3.1129E-01
7	6.0653E+00	1.1715E+00	3.3873E-01	2.4137E-01
8	4.9659E+00	1.1082E+00	3.2521E-01	2.7623E-01
9	3.6788E+00	1.0339E+00	3.3469E-01	1.8660E-01
10	3.0119E+00	9.8682E-01	3.5273E-01	9.9863E-02
11	2.7253E+00	9.5186E-01	3.5385E-01	6.8684E-02
12	2.4660E+00	9.2505E-01	3.4291E-01	7.2357E-02
13	2.3653E+00	9.1570E-01	3.3654E-01	6.6472E-02
14	2.3457E+00	9.0478E-01	3.2745E-01	6.1132E-02
15	2.2313E+00	8.6752E-01	2.8999E-01	2.1297E-02
16	1.9205E+00	8.0707E-01	2.2777E-01	3.8088E-03
17	1.6530E+00	7.4286E-01	1.6956E-01	5.7312E-04
18	1.3534E+00	6.5890E-01	1.0091E-01	5.5073E-05
19	1.0026E+00	5.7861E-01	4.8582E-02	1.3126E-06
20	8.2085E-01	4.9185E-01	2.7786E-02	0.
21	7.4274E-01	3.2307E-01	1.4531E-02	0.
22	6.0810E-01	1.9477E-01	6.5054E-03	0.
23	4.9787E-01	1.3666E-01	2.1654E-03	0.
24	3.6883E-01	1.0314E-01	1.4947E-04	0.
25	2.9721E-01	6.5891E-02	0.	0.
26	1.8316E-01	2.3016E-02	0.	0.
27	1.1109E-01	5.3395E-03	0.	0.
28	6.7379E-02	1.6339E-03	0.	0.
29	4.0868E-02	3.5776E-06	0.	0.
30	3.1828E-02	0.	0.	0.
31	2.6058E-02	0.	0.	0.
32	2.4176E-02	0.	0.	0.
33	2.1875E-02	0.	0.	0.
34	1.5034E-02	0.	0.	0.
35	7.101/E-03	0.	0.	0.
36	3.35468-03	0.	0.	0.
37	1.5846E-03	0.	0.	0.
38	4.5400E-04	0.	0.	0.
39	2.1445E-04	0.	0.	0.
40	1.0130E-04 2.7266E-05	0.	0.	0.
41	1 0677E-05	0.	0.	0.
4Z 10	5 0435F-06	0.	0.	0.
43	1 855/F-06	0.	0.	0.
44	1.0554E-00 8 7643F-07	0.	0.	0.
45	4 1399E-07	0	0	0
40	1.0000E-07	0	0	0
	1.0000E-11	•••	••	



3.5 - U-235 Fission Neutron Spectra

The U-235 fission neutron spectra (χ) used to obtain the PCA-Replica neutron source in the fixed source transport calculations (see Chapter 4) are reported in TAB. 3.7.

It is underlined that, whereas the U-235 fission spectrum data included in the package of the ORNL BUGLE-96 /7/ library refer only to prompt neutrons, the U-235 fission spectrum data contained respectively in the packages of the ENEA-Bologna BUGJEFF311.BOLIB /2/ and BUGENDF70.BOLIB /3/ similar libraries are total fission spectra, i.e. they include the contributions of both prompt and delayed neutrons. This option was made available through the use of the ENEA-Bologna 2007 Revision /28/ of the ORNL SCAMPI /29/ nuclear data processing system, freely released at OECD-NEADB and ORNL-RSICC.

Graphical representations of the U-235 total fission neutron spectra (χ) for the BUGJEFF311.BOLIB and BUGENDF70.BOLIB libraries together with the U-235 prompt fission neutron spectrum (χ) for the BUGLE-96 library are reported in FIG. 3.4 and 3.5.



TAB. 3.7

Total or Prompt U-235 Fission Neutron Spectra (χ) Used in the TORT-3.2 Calculations Using the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 Libraries

Group	Upper Energy [MeV]	Total (χ) U-235 BUGJEFF311.BOLIB	Total (χ) U-235 BUGENDF70.BOLIB	Prompt (χ) U-235 BUGLE-96
1	1.7332E+01	4.9847E-05	4.9839E-05	5.0179E-05
2	1,4191E+01	2.0032E-04	2.0031E-04	2.0166E-04
3	1 2214E+01	1 1384E = 03	1 1384E = 03	1 1460E - 03
4	1.0000E+01	2 5055E-03	2 5055E-03	25222E-03
5	8 6071E+00	5 6193E-03	5 6195E-03	5 6568E-03
6	7 4082E+00	1 6040E - 02	1 6041E = 02	1 6147E = 02
7	6 0653E+00	3.0508E-02	3 0511E - 02	3 0712E - 02
, 8	4 9659E+00	7 9978E - 02	7 9986E-02	8 0512E-02
9	3 6788E+00	7.6252E - 02	7 6258E-02	7 6758E - 02
10	3 0119E+00	4 3722E-02	4 3728E-02	4 4010E - 02
10	2.7253E+00	4 6381E-02	4 63888-02	4.6685E-02
12	2.7255E+00 2.4660E+00	1 9899E - 02	1 9903E-02	2.0028E-02
13	2.3653F+00	4 00048-03	4 0013E-03	A 0262E-03
14	2.3055100 2.3457E+00	2.4188F-02	$\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$	2.4344F=02
14	2.3437E+00 2.2213E+00	2.4100E-02 7 3086F-02	7 3105F-02	2.4344E-02 7 3547E-02
15	2.2313E+00 1 9205F+00	7.30008-02	7.15388-02	7.3347E=02 7.1946F=02
10	1.9203E+00	9 9032E-02	9 9093E-02	9 9/95F-02
10	1 353/5+00	0.9032E-02 1 1467E-01	8.9083E-02 1 1474F-01	0.9495E-02 1 1503F-01
18	1 00262+00	1.1407E-01 6.2706E-02	1.14/4E-01 6 272/E-02	1.1505E-01 6.2695E-02
19	1.0020E+00 9.2095E-01	0.2700E-02 2 7227E-02	0.2/34E-02 2 7220E-02	0.2005E-02 2 7230E-02
20	0.2003E-01		2.7329E-02	
21	7.42/4E-UI		4.7130E-02	4.0051E-02
22	6.0810E-01		3.8038E-02	3.76ISE-02
23	4.9/8/E-01	4.2477E-02	4.2436E-02	4.1771E-02
24	3.6883E-01	2.1827E-02	2.180/E-02	2.1390E-02
25	2.9/2IE-01	3.0837E-02	3.0779E-02	3.0048E-02
26	1.8316E-01		1.5922E-02	
27	1.1109E-01	7.7422E-03	7.7147E-03	7.4251E-03
28	6./3/9E-U2	3.7043E-03	3.6943E-03	3.5461E-03
29	4.0868E-02	1.0482E-03	1.0459E-03	9.9806E-04
30	3.1828E-02	6.0/3/E-04	6.03/4E-04	5.6977E-04
31	2.6058E-02	1.8654E-04	1.8501E-04	1./33/E-04
32	2.41/6E-02	2.1922E-04	2.1/35E-04	2.0305E-04
33	2.18/5E-02	5.9716E-04	5.8/81E-04	5.403/E-04
34	1.5034E-02	5.38/5E-04	5.3054E-04	4.8419E-04
35	7.1017E-03	1.7068E-04	1.7033E-04	1.5746E-04
36	3.3546E-03	5.7556E-05	5.7386E-05	5.1156E-05
37	1.5846E-03	2.4994E-05	2.4884E-05	2.0827E-05
38	4.5400E-04	3.4437E-06	3.4200E-06	2.5484E-06
39	2.1445E-04	1.2527E-06	1.2414E-06	8.2729E-07
40	1.0130E-04	5.5078E-07	5.4440E-07	3.0900E-07
41	3.7266E-05	1.7589E-07	1.7323E-07	5.9997E-08
42	1.0677E-05	2.2718E-08	2.9006E-08	5.4050E-12
43	5.0435E-06	1.2140E-08	1.3842E-08	0.
44	1.8554E-06	3.7279E-09	3.8754E-09	0.
45	8.7643E-07	1.7610E-09	1.7694E-09	0.
46	4.1399E-07	1.1957E-09	1.1790E-09	0.
47	1.0000E-07	3.8080E-10	3.7167E-10	0.
	1.0000E-11			





di



L

ENEN



4 - TRANSPORT CALCULATIONS

4.1 - Transport Calculation General Features

The whole PCA-Replica experimental array (see /9/ and 2.1) was reproduced with the TORT-3.2 /13/ three-dimensional (3D) discrete ordinates (S_N) code included in the ORNL DOORS-3.2 /14/ system of deterministic codes.

The TORT-3.2 code was used on a personal computer (CPU: INTEL PENTIUM D 3.40 GHz, 3.10 GB of RAM) under Linux openSUSE 10.2 (i586) operating system with FORTRAN-77 compiler g77, version 3.3.5-38.

The ENEA-Bologna ADEFTA-4.1 /17/ program was employed in the calculation of the atomic densities of the isotopes involved in the compositional model on the basis of the atomic abundances reported in the BNL-NNDC database /33/ included in ADEFTA. This calculation was necessary since the atomic densities of the PCA-Replica experiment, indicated in the official material composition in TAB. 2.2 (derived from TAB. 3 of reference /9/), are given for natural element except for the two uranium isotopes U-235 and U-238.

The automatic generation of the spatial mesh grid and the graphical verification of the PCA-Replica benchmark experiment geometrical model for TORT-3.2 were performed through the ENEA-Bologna BOT3P-5.3 /18/ pre/post-processor system.

In all the calculations it was reproduced the whole three-dimensional PCA-Replica experimental array in the (X,Y,Z) Cartesian geometry in order to assure a proper detailed description of the spatial heterogeneity of the neutron source emitted by the fission plate.

In particular it was described a parallelepiped geometry (whose dimensions were $185.08 \times 180.0 \times 180.0$ cm, respectively along the X, Y and Z axis) with a $65X \times 63Y \times 182Z$ fine spatial mesh grid, where Z was the horizontal nuclear axis (see FIGs. 2.3 and 2.6) where the dosimeter measure positions were located. Volumetric meshes with sides always inferior to 0.5 cm were described along the Z axis to obtain the best accuracy in the calculations.

The horizontal section (at Y = 0.0 cm) of the PCA-Replica compositional and geometrical model reproduced in all the TORT-3.2 (X,Y,Z) calculations is reported in FIG. 4.1 together with the dosimeter locations.

The ENEA-Bologna BUGJEFF311.BOLIB /2/ (JEFF-3.1.1 /4/ /5/ data) and BUGENDF70.BOLIB /3/ (ENDF/B-VII.0 /6/ data) working libraries were alternatively used in the transport calculations with TORT-3.2 together with the ORNL BUGLE-96 /7/ (ENDF/B-VI.3 /8/ data) working library assumed as a reliable standard library for the neutron dose and neutron spectrum calculated results. A brief description of each previously cited library is reported in Chapter 3 (see respectively 3.1, 3.2 and 3.3).

All the calculations were performed only with the first 29 neutron groups (see TAB. 3.1), above 3.1828E+04 eV, since all the neutron energy thresholds (see 2.3 and TAB. 2.4) of the three employed dosimeters are above this energy value.

It is underlined that it was not possible to use the same set of atomic densities in all the calculations with the three previously cited libraries. In fact the BUGJEFF311.BOLIB and BUGENDF70.BOLIB libraries include all the needed processed cross sections for all the isotopes of each natural element involved in the PCA-Replica compositional model whereas, on the contrary, this possibility is not always assured for the BUGLE-96 library. Several processed cross sections needed in the description of the PCA-Replica compositional model are in fact available in BUGLE-96 only as natural element cross section files.


In particular the common set of atomic densities used in the calculations with the BUGJEFF311.BOLIB and BUGENDF70.BOLIB libraries is reported in TAB. 4.1 while the different set of atomic densities shown in TAB. 4.2 was used in the calculations with the BUGLE-96 library.

Both infinite dilution and self-shielded cross sections were selected. Self-shielded cross sections from the three library packages were used when available. In particular it is underlined that the thermal shield (stainless steel) and the pressure vessel (mild steel) simulators of the PCA-Replica experiment were characterized by atomic densities quite similar to those used to calculate the background cross sections employed in the self-shielding of the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 neutron cross sections. Group-organized files of macroscopic cross sections, requested by TORT-3.2 and derived from the cited working libraries in FIDO-ANISN format, were prepared through the ORNL GIP (see /14/) program, specifically dedicated to the discrete ordinates transport codes (ANISN-ORNL, DORT, TORT) of the DOORS system. The ENEA-Bologna ADEFTA-4.1 program was used not only to calculate the atomic densities for the benchmark experiment compositional model but also to handle them properly in order to automatically prepare the macroscopic cross section sets of the compositional model material mixtures in the format required by GIP.

Fixed source transport calculations with one source (outer) iteration were performed using fully symmetrical discrete ordinates directional quadrature sets for the flux solution.

The P_3 - S_8 approximation was adopted as the standard reference. P_N corresponds to the order of the expansion in Legendre polynomials of the scattering cross section matrix and S_N represents the order of the flux angular discretization. It is underlined that the P_3 - S_8 approximation is the most widely used option in the fixed source calculations dedicated to LWR safety analyses.

A further parametric analysis was carried out on the P_N and S_N orders. P_3 calculations were performed with different sets of fully symmetrical quadrature for the S_8 , S_{12} and S_{16} orders of the flux angular discretization. Similarly, P_5 calculations were performed with different sets of fully symmetrical quadrature for the S_{12} and S_{16} orders of the flux angular discretization. The BUGJEFF311.BOLIB library was exclusively used to perform this parametric analysis.

The theta-weighted difference approximation was selected for the flux extrapolation model. In all the calculations the same numerical value (1.0E-03) for the point-wise flux convergence criterion was employed.

The vacuum boundary condition was selected at the left, right, inside, outside, bottom and top geometrical boundaries.

The IRDF-2002 /16/ derived (see /15/ and 3.4) flat weighting neutron dosimeter cross sections in the BUGLE-96 47-group neutron energy structure for the Rh-103(n,n')Rh-103m, In-115(n,n')In-115m and S-32(n,p)P-32 nuclear reactions were used in all the calculations with the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 libraries to obtain the corresponding reaction rates in all the experimental dosimeter positions in water, steel and air. The use of the IRDF-2002 derived (see /15/ and 3.4) 1/4 T RPV weighting neutron dosimeter cross sections was properly limited, alternatively with the flat weighting cross sections, to obtain the dosimetric results in the measure positions (1/4 T RPV and 3/4 T RPV) located inside the mild steel RPV simulator.



Finally, in order to calculate with proper accuracy the neutron fluxes above 0.1, 1.0 and 3.0 MeV using the three libraries, the neutron flux contributions of the groups No. 27, No. 19 and No. 10 were respectively corrected by multiplying the cited group contributions by the following factors reported herewith (see TAB. B1 and pages 161-162 of reference /2/; see TAB. B1 and pages 167-168 of reference /3/; see TAB. 3.14 and page 66 of reference /7/), taking into account that the lower energy limits of the cited neutron groups do not correspond respectively to the 0.1, 1.0 and 3.0 MeV neutron energies.

Neutron Flux > 0.1 MeV

Group No. 27 Factor = $2.1034\text{E}-01 = \ln(\text{E}_0/\text{E}_g)/\ln(\text{E}_{g+1}/\text{E}_g)$ where:

$$\begin{split} E_0 &= 0.1 \text{ [MeV]};\\ E_g &= 1.1109\text{E-}01 \text{ [MeV]} \text{ (Upper energy limit group No. 27);}\\ E_{g^{+1}} &= 6.7379\text{E-}02 \text{ [MeV]} \text{ (Lower energy limit group No. 27).} \end{split}$$

Neutron Flux > 1.0 MeV

Group No. 19 Factor = $1.3000\text{E}-02 = \ln(\text{E}_0/\text{E}_g) / \ln(\text{E}_{g+1}/\text{E}_g)$ where:

 $E_0 = 1.0 \text{ [MeV]};$ $E_g = 1.0026 \text{ [MeV]}$ (Upper energy limit group No. 19); $E_{g+1} = 0.82085 \text{ [MeV]}$ (Lower energy limit group No. 19).

Neutron Flux > 3.0 MeV

Group No. 10 Factor = $3.959\text{E}-02 = \ln(\text{E}_0/\text{E}_g) / \ln(\text{E}_{g+1}/\text{E}_g)$ where:

$$\begin{split} E_0 &= 3.0 \text{ [MeV]};\\ E_g &= 3.0119 \text{ [MeV]} \text{ (Upper energy limit group No. 10);}\\ E_{g^{+1}} &= 2.7253 \text{ [MeV]} \text{ (Lower energy limit group No. 10).} \end{split}$$



FIG. 4.1

PCA-Replica - Compositional and Geometrical Model in the TORT-3.2 (X,Y,Z) Calculations.







TAB. 4.1

PCA-Replica - Atomic Densities Used in the TORT-3.2 Calculations Using the BUGJEFF311.BOLIB and BUGENDF70.BOLIB Libraries.

Material	Material Density $[g \times cm^{-3}]$	Element	Isotopic Abundance	Atomic Density [atoms \times barn ⁻¹ \times cm ⁻¹]
Graphite	1.65	C-nat ^a	1.	8.27600E-02
	2.70	41.07	1	
Aluminium Cladding	2.70	AI-27	1.	6.02900E-02
Alloy Fuel ^b	3.257	Al-27	1.	5.81800E-02
		U-235	0.93	1.55200E-03
		U-238	0.07	1.15400E-04
Water	1.0	H-1	1.	6.68800E-02
		O-16	1.	3.34400E-02
Stainless Steel	7.88	C-nat	1.	6.72100E-05
		Si-28	0.92230	6.86007E-04
		Si-29	0.04683	3.48322E-05
		Si-30	0.03087	2.29611E-05
		Mn-55	1.	1.35600E-03
		P-31	1.	3.83200E-05
		S-32	0.95020	8.44158E-06
		S-33	0.00750	6.66300E-08
		S-34	0.04210	3.74016E-07
		S-36	0.00020	1.77680E-09
		Cr-50	0.04345	7.33436E-04
		Cr-52	0.83789	1.41436E-02
		Cr-53	0.09501	1.60377E-03
		Cr-54	0.02365	3.99212E-04
		Ni-58	0.68077	5.17453E-03
		Ni-60	0.26223	1.99321E-03
		Ni-61	0.01140	8.66514E-05
		Ni-62	0.03634	2.76220E-04
		Ni-64	0.00926	7.03853E-05
		Mo-92	0.14840	2.71720E-05
		Mo-94	0.09250	1.69368E-05
		Mo-95	0.15920	2.91495E-05
		Mo-96	0.16680	3.05411E-05
		Mo-97	0.09550	1.74861E-05
		Mo-98	0.24130	4.41820E-05
		Mo-100	0.09630	1.76325E-05
		Ti-46	0.08250	7.35900E-07
		1		1



TAB. 4.1 Continued

PCA-Replica - Atomic Densities Used in the TORT-3.2 Calculations Using the BUGJEFF311.BOLIB and BUGENDF70.BOLIB Libraries.

Material	Material Density $[g \times cm^{-3}]$	Element	Isotopic Abundance	Atomic Density [atoms \times barn ⁻¹ \times cm ⁻¹]
		Ti-47 Ti-48 Ti-49 Ti-50 Nb-93 Cu-63 Cu-65 Fe-54	0.07440 0.73720 0.05410 0.05180 1. 0.69170 0.30830 0.05845	6.63648E-07 6.57582E-06 4.82572E-07 4.62056E-07 7.15400E-06 1.24022E-04 5.52782E-05 3.45381E-03
		Fe-56 Fe-57 Fe-58	0.91754 0.02119 0.00282	5.42174E-02 1.25212E-03 1.66634E.04
Mild Steel	7.835	C-nat Mn-55 P-31 S-32 S-33 S-34 S-36 Fe-54 Fe-56 Fe-57 Fe-58	1. 1. 1. 0.95020 0.00750 0.04210 0.00020 0.05845 0.91754 0.02119 0.00282	8.64600E-04 9.36600E-04 1.52400E-05 4.47639E-05 3.53325E-07 1.98333E-06 9.42200E-09 4.87356E-03 7.65045E-02 1.76682E-03 2.35132E-04
Concrete	2.3	Si-28 Si-29 Si-30 Fe-54 Fe-56 Fe-57 Fe-58 H-1 O-16 A1-27 Ca-40 Ca-42 Ca-43	0.92230 0.04683 0.03087 0.05845 0.91754 0.02119 0.00282 1. 1. 1. 1. 1. 0.96941 0.00647 0.00135	3.79988E-02 1.92940E-03 1.27184E-03 5.03196E-05 7.89910E-04 1.82425E-05 2.42774E-06 3.40700E-02 1.13500E-01 4.32700E-03 3.65468E-03 2.43919E-05 5.08950E-06



TAB. 4.1 Continued

PCA-Replica - Atomic Densities Used in the TORT-3.2 Calculations Using the BUGJEFF311.BOLIB and BUGENDF70.BOLIB Libraries.

Material	Material Density $[g \times cm^{-3}]$	Element	Isotopic Abundance	Atomic Density [atoms \times barn ⁻¹ \times cm ⁻¹]
Air	0.001205°	Ca-44 Ca-46 Ca-48 Na-23 K-39 K-40 K-41 N-14 N-14 N-15 O-16	0.02086 0.00004 0.00187 1. 0.932581 0.000117 0.067302 0.99634 0.00366 1.	7.86422E-05 1.50800E-07 7.04990E-06 2.39000E-03 1.31028E-03 1.64385E-07 9.45593E-05 3.95960E-05 1.45454E-07 1.05642E-05

(^a) (^b) (^c) C-nat means carbon natural element.

Uranium enriched to 93 w% in U-235.

Air density at the temperature of 20.0 °C taken from "Air Properties" in www.engineeringtoolbox.com.



TAB. 4.2

PCA-Replica - Atomic Densities Used in the TORT-3.2 Calculations Using the BUGLE-96 Library.

Material	Material Density $[g \times cm^{-3}]$	Element	Isotopic Abundance	Atomic Density [atoms \times barn ⁻¹ \times cm ⁻¹]
Graphite	1.65	C-nat ^a	1.	8.27600E-02
Aluminium Cladding	2.70	Al-27	1.	6.02900E-02
Alloy Fuel ^b	3.257	Al-27	1.	5.81800E-02
-		U-235	0.93	1.55200E-03
		U-238	0.07	1.15400E-04
Water	1.0	H-1	1.	6.68800E-02
		O-16	1.	3.34400E-02
Stainless Steel	7.88	C-nat	1.	6.72100E-05
		Si-nat	1.	7.43800E-04
		Mn-55	1.	1.35600E-03
		P-31	1.	3.83200E-05
		S-nat	1.	8.88400E-06
		Cr-50	0.04345	7.33436E-04
		Cr-52	0.83789	1.41436E-02
		Cr-53	0.09501	1.60377E-03
		Cr-54	0.02365	3.99212E-04
		Ni-58	0.68077	5.17453E-03
		Ni-60	0.26223	1.99321E-03
		Ni-61	0.01140	8.66514E-05
		Ni-62	0.03634	2.76220E-04
		Ni-64	0.00926	7.03853E-05
		Mo-nat	1.	1.83100E-04
		Ti-nat	1.	8.92000E-06
		Nb-93	1.	7.15400E-06
		Cu-63	0.69170	1.24022E-04
		Cu-65	0.30830	5.52782E-05
		Fe-54	0.05845	3.45381E-03
		Fe-56	0.91754	5.42174E-02
		Fe-57	0.02119	1.25212E-03
		Fe-58	0.00282	1.66634E-04



TAB. 4.2 Continued

PCA-Replica - Atomic Densities Used in the TORT-3.2 Calculations Using the BUGLE-96 Library.

Material	Material Density $[g \times cm^{-3}]$	Element	Isotopic Abundance	Atomic Density [atoms \times barn ⁻¹ \times cm ⁻¹]
M:1104-1	7.925	C ret	1	
Mild Steel	1.835	C-nat	l. 1	8.64600E-04
		Mn-55	l. 1	9.36600E-04
		P-31	l.	1.52400E-05
		S-nat	l.	4.71100E-05
		Fe-54	0.05845	4.87356E-03
		Fe-56	0.91754	7.65045E-02
		Fe-57	0.02119	1.76682E-03
		Fe-58	0.00282	2.35132E-04
Concrete	2.3	Si-nat	1.	4.12000E-02
		Fe-54	0.05845	5.03196E-05
		Fe-56	0.91754	7.89910E-04
		Fe-57	0.02119	1.82425E-05
		Fe-58	0.00282	2.42774E-06
		H-1	1.	3.40700E-02
		O-16	1.	1.13500E-01
		Al-27	1.	4.32700E-03
		Ca-nat	1.	3.77000E-03
		Na-23	1.	2.39000E-03
		K-nat	1.	1.40500E-03
Air	0.001205°	N 14	0.00634	
All	0.001203	IN-14	0.99034	3.95960E-05
		N-15	0.00300	1.45454E-07
		U-16	1.	1.05642E-05

(a) C-nat means carbon natural element.

(b) Uranium enriched to 93% in U-235.

(c) Air density at the temperature of 20.0 °C taken from "Air Properties" in <u>www.engineeringtoolbox.com</u>.



4.2 - PCA-Replica Fission Neutron Source

As previously reported, a precise inhomogeneous fission neutron source distribution (see TAB. 2.3) in the fission plate (see FIG. 2.4) was adopted, following the recommended official specifications (see TAB. A6 and FIG. A1 of reference /9/).

The distributed (or volumetric) fission neutron sources used in the calculations with the BUGJEFF311.BOLIB /2/, BUGENDF70.BOLIB /3/ and BUGLE-96 /7/ libraries were obtained using respectively their corresponding fission neutron spectra reported in TAB. 3.7 (see 3.5).

The BUGJEFF311.BOLIB U-235 total (prompt + delayed) fission neutron spectrum (χ) data derived from JEFF-3.1.1 are reported in TAB. 3.7 and are identical to those shown in the TAB. C.1 of reference /2/ at page 165.

The BUGENDF70.BOLIB U-235 total (prompt + delayed) fission neutron spectrum (χ) data derived from ENDF/B-VII.0 are reported in TAB. 3.7 and are identical to those shown in the TAB. C.1 of reference /3/ at page 171.

The BUGLE-96 U-235 prompt fission neutron spectrum (χ) data derived from ENDF/B-VI.3 are reported in TAB. 3.7 and are identical to those shown in the TAB. 3.14 of reference /7/ at page 58. The total fission neutron spectrum data are not available in the BUGLE-96 library (see 3.5).

In order to determine the volumetric neutron source for each transport calculation with the three libraries, the common value of \overline{v} (U-235) = 2.437 was used for the average number of neutrons produced per U-235 thermal fission, as suggested in the official description (see page 49 of reference /9/) of the PCA-Replica experiment. This choice was addressed also to assure the consistent comparison of the calculated results.

4.2.1- Inhomogeneous Neutron Source

In the TORT calculations with the inhomogeneous neutron source, the 6.74E-04 fission plate Watts per NESTOR Watt numerical value (see page 48 of reference /9/) was given to the "xnf" source multiplier parameter in the 67** "problem parameters" array. The numerical values given to the 96** "distributed source distribution" array correspond to

The numerical values given to the 96** "distributed source distribution" array correspond to the numerical values reported in TAB. 2.3 (derived from TAB. A6 of reference /9/), representing the fission plate neutron source spatial distribution.

4.2.2 - Homogeneous Neutron Source

In the TORT calculations with the homogeneous neutron source the "xnf" source multiplier parameter in the 67** "problem parameters" array was calculated as follows.

 $xnf = A \times \overline{\nu} (U-235) / V_p = 3.3477E+04,$

where

A = 2.104E+07 fissions \times s⁻¹ \times NESTOR Watt⁻¹, fission plate total fission rate per NESTOR Watt (see page 48 of reference /9/);

 \overline{v} (U-235) = 2.437, average number of neutrons emitted per thermal fission (see page 49 of reference /9/);

 $V_p = 40.2 \times 63.5 \times 0.6 = 1531.62 \text{ cm}^3$, fission plate alloy fuel volume.



This choice is consistent with the numerical values given to the 96^{**} "distributed source distribution" array where a unit neutron source density (1 neutron \times cm⁻³ \times s⁻¹) was attributed to all the spatial cells corresponding to the fission plate alloy fuel volume. Therefore the total fission neutron source strength calculated by TORT through the 96^{**} array and the xnf parameter is numerically equal to xnf \times V_p.



5 - DISCUSSION OF THE RESULTS

The PCA-Replica 12/13 neutron dose and neutron spectrum calculated results are compared with the corresponding experimental results in the present chapter.

Two normalizations for the dosimetric and the spectral integral results were used to report the relative data on tables or to represent them graphically on figures: to 1 Watt of the fission plate or, alternatively, to 1 Watt of the NESTOR reactor. The conversion factor from the first normalization to the second one is equal to 6.74E-04 fission plate Watts per NESTOR Watt (see page 48 of reference /9/), i.e. the numerical value given in the first normalization must be multiplied by the conversion factor to obtain the corresponding numerical value in the second normalization.

It is underlined that the two cited normalizations were both used in reference /9/ to represent the same type of results. For example, the Rh-103(n,n'), In-115(n,n') and S-32(n,p) experimental reaction rates are reported in the TAB. 6 of reference /9/ per NESTOR Watt whilst, on the contrary, the Rh-103(n,n') calculated and experimental reaction rates in the FIG. 10 of reference /9/ are shown per fission plate Watt, as well as the dosimetric results reported in the TAB. 14 of reference /9/. The neutron spectrum results are shown in the FIGs. 7, 8 and 9 of reference /9/ per fission plate Watt whilst, on the contrary, the experimental neutron spectra in the TAB. 7 of reference /9/ are reported per NESTOR Watt.

In the present work it was followed an approach addressed to assure the consistency between the tabular and graphical representations of the calculated/experimental results chosen in reference /9/ and those adopted in the present analysis. In other words it was decided to maintain in the present work, for the results included in a specific table or figure, the same normalization adopted in the corresponding table or figure of reference /9/ in order to have the possibility to make an easier comparison of the dosimetric or spectral results.

5.1 - Dosimetric Results

The experimental dosimetric results (see 2.3) were obtained in PCA-Replica 12/13 with three threshold activation dosimeters located in ten measure positions. In particular the Rh-103(n,n')Rh-103m dosimeters were positioned in all ten measure positions located in the water gaps, in the mild steel RPV and in the void box filled with air. The In-115(n,n')In-115m and S-32(n,p)P-32 dosimeters were placed only in three measure positions in the RPV and in the void box.

The calculated reaction rate results obtained with the flat weighted dosimeter cross sections and the realistic inhomogeneous neutron source are reported in TAB. 5.1 and FIG. 5.1 for Rh-103(n,n')Rh-103m, in TAB. 5.2 and FIG. 5.2 for In-115(n,n')In-115m and in TAB. 5.3 and FIG. 5.3 for S-32(n,p)P-32. The experimental reaction rates reported in the TABs. 5.1, 5.2 and 5.3 were taken from the TAB. 6 of reference/9/. It is underlined that the "as measured" experimental reaction rates reported in the previously cited tables contain a contribution from the NESTOR core neutron leakage background. Since the calculated (C) reaction rates refer only to the neutrons produced in the fission plate per 1 Watt of NESTOR power, the "as measured" experimental (E) reaction rate values in the C/E ratios are reduced (see 2.3) by 4% in the RPV and void box measure positions and by 2% in the measure positions of the two water gaps, as recommended at page 10 of reference /9/. All the calculated results reported in the previously cited tables and figures were obtained using the three libraries



BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 and the TORT-3.2 code in P_3 -S₈ approximation. Concerning the Rh-103(n,n')Rh-103m dosimeters, only few calculated results, obtained with the three cited libraries in the second water gap, present underestimated values slightly outside the range of deviation of ±10% from the corresponding experimental results. The deviations of the calculated results for the In-115(n,n')In-115m and S-32(n,p)P-32 dosimeters are always contained within ±10% of the corresponding experimental results, available only in the RPV and void box measure positions. The calculated results obtained using the BUGJEFF311.BOLIB and BUGENDF70.BOLIB libraries appear in general to be almost always slightly overstimated with respect to the corresponding BUGLE-96 calculated results.

Since the Rh-103(n,n')Rh-103m dosimeters were employed in all ten measure positions in the PCA-Replica 12/13 experiment, it was possible to show in FIG. 5.4 (see also for comparison FIG. 10 of reference /9/) a subjective trend line over the whole range of neutron penetration (about four decades of reaction rate attenuation). This trend line connects all the Rh-103(n,n')Rh-103m experimental reaction rates compared with the corresponding calculated reaction rates obtained using the BUGJEFF311.BOLIB library.

The use of the IRDF-2002 derived (see /15/ and 3.4) 1/4 T RPV weighting neutron dosimeter cross sections, properly limited to obtain (see 4.1) calculated dosimetric results in the measure positions (1/4 T RPV and 3/4 T RPV) located inside the mild steel RPV simulator, did not give meaningful differences with respect to the corresponding calculated results obtained with the IRDF-2002 derived flat weighting neutron dosimeter cross sections.

Adopting the same normalization indicated in the TABs. 5.1, 5.2 and 5.3, i.e. reaction rates per NESTOR reactor Watt, the spatial distributions of the Rh-103(n,n'), In-115(n,n') and S-32(n,p) reaction rates in the PCA-Replica horizontal section at Y = 0.0 cm (see FIG. 4.1) are shown respectively in the FIGs. 5.5, 5.6 and 5.7.

The spatial distributions of the neutron fluxes with the same normalization per NESTOR reactor Watt used previously for the reaction rates are shown in the PCA-Replica horizontal section at Y = 0.0 cm (see FIG. 4.1) for neutron fluxes with neutron energies above 0.1, 1.0 and 3.0 MeV, respectively in the FIGs. 5.8, 5.9 and 5.10.

The reaction rate and the neutron flux spatial distributions reported in the previously cited figures were obtained with the BUGJEFF311.BOLIB library and the TORT-3.2 code in P_3 -S₈ approximation using the inhomogeneous neutron source.

It is underlined that, in practice, the results coming from Rh-103(n,n') correspond to neutron fluxes above about 0.1 MeV, the results coming from In-115(n,n') to neutron fluxes above about 1.0 MeV and the results coming from S-32(n,p) to neutron fluxes above about 3.0 MeV (see also /25/ and TAB. 2.4).

As useful complementary data of further analysis, the fast neutron flux damage parameters for neutron energies E above 0.1, 1.0 and 3.0 MeV, calculated with the three BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 libraries, are reported in TAB. 5.4 in each of the ten measure positions plus the 1/2 T RPV position, not used for the PCA-Replica 12/13 neutron dose and spectrum measures. The normalization of the neutron fluxes to 1 Watt of the NESTOR reactor was adopted to represent the calculated results in a consistent way with the FIGs. 5.8, 5.9 and 5.10, representing respectively the spatial distributions of the previously cited fast neutron fluxes. The flux ratios of the previously cited calculated fast neutron fluxes at the same ten plus one previously cited positions are reported in TAB. 5.5. The neutron flux ratios Φ (E > 1.0 MeV)/ Φ (E > 0.1 MeV),



 Φ (E > 3.0 MeV)/ Φ (E > 0.1 MeV) and Φ (E > 3.0 MeV)/ Φ (E > 1.0 MeV) were obtained from calculations performed with the three BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 libraries and the TORT-3.2 code in P₃-S₈ approximation using the inhomogeneous neutron source.

The effect of the use of the inhomogeneous and homogeneous neutron sources was tested and compared through TORT-3.2 calculations in P_3 -S₈ approximation, performed with the exclusive use of the BUGJEFF311.BOLIB library.

The relative results obtained are reported and compared in TAB. 5.6 and FIG. 5.11 for Rh-103(n,n')Rh-103m, in TAB. 5.7 and FIG. 5.12 for In-115(n,n')In-115m and in TAB. 5.8 and FIG. 5.13 for S-32(n,p)P-32. The use of the realistic inhomogeneous spatial distribution of the neutron source implies a systematic slight (few percents) overestimation (see the previously cited tables and figures) of the calculated results of all the dosimeters in comparison with the corresponding calculated results obtained with the simplified homogeneous spatial distribution of the neutron source.

The C/E results of the parametric analysis on the P_N and S_N orders of approximation (see 4.1) are reported in the FIGs. 5.14 and 5.15 for Rh-103(n,n')Rh-103m, in the FIGs. 5.16 and 5.17 for In-115(n,n')In-115m and in the FIGs. 5.18 and 5.19 for S-32(n,p)P-32. The results shown in the previously cited figures are given only for two key measure positions: 1/4 T RPV (mild steel) and void box (air). To perform this parametric analysis it was decided to use TORT-3.2 exclusively with the BUGJEFF311.BOLIB library and the inhomogeneous fission neutron source. In the FIGs. 5.14, 5.16 and 5.18 reporting the results of the P₃ calculations it is possible to note, in the results of the S₈ calculations, slight C/E differences for all the dosimeters with respect to the corresponding C/E values obtained from the S₁₂ and S₁₆ calculations which, on the contrary, give C/E results fully stabilized for all the dosimeters. In the FIGs. 5.15, 5.17 and 5.19 reporting the results of the P₅ calculations, all the C/E results appear completely stabilized for all the dosimeters, i.e. no meaningful C/E difference for a given dosimeter is evident between the corresponding results of the S₁₂ and S₁₆ calculations.



TAB. 5.1

PCA-Replica - Summary of Experimental (E) and Calculated (C) Rh-103(n,n') Reaction Rates^a per NESTOR Reactor Watt along the Horizontal Axis Z.

P₃-S₈ Calculations Using the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 Libraries and the Inhomogeneous Neutron Source.

Dos	Distance from Fission	Experimental Reaction Rate ^a \pm Random Error (1 σ)	BUGJEFF311.E Calculatio	BOLIB n	BUGENDF70.E Calculatio	BOLIB n	BUGLE-9 Calculatio	6 n	Reference
Pos.	Plate on the Axis Z [cm]	(E) Systematic Error ± 3.0%	Calculated Reaction Rate ^a (C)	C/E ^b	Calculated Reaction Rate ^a (C)	C/E ^b	Calculated Reaction Rate ^a (C)	C/E ^b	Location
1	1.91	1.69E-20 ± 3.0%	1.81E-20	1.09	1.81E-20	1.09	1.82E-20	1.10	
2	7.41	3.78E-21 ± 3.0%	3.43E-21	0.93	3.44E-21	0.93	3.44E-21	0.93	12 cm
3	12.41	1.40E-21 ± 3.0%	1.30E-21	0.95	1.31E-21	0.95	1.30E-21	0.95	Water Gap 1
4	14.01	1.27E-21 ± 3.0%	1.15E-21	0.93	1.16E-21	0.93	1.15E-21	0.93	
5	19.91	4.23E-22 ± 3.0%	4.18E-22	1.01	4.17E-22	1.00	4.11E-22	0.99	
6	25.41	1.15E-22 ± 4.0%	1.02E-22	0.91	1.02E-22	0.91	1.01E-22	0.89	13 cm Water Gap 2
7	30.41	4.73E-23 ± 4.0%	4.12E-23	0.89	4.13E-23	0.89	4.06E-23	0.88	
8	39.01	2.07E-23 ± 1.0%	2.02E-23	1.02	2.02E-23	1.01	1.98E-23	1.00	1/4 T RPV
9	49.61	5.53E-24 ± 1.9%	5.62E-24	1.06	5.59E-24	1.05	5.45E-24	1.03	3/4 T RPV
10	58.61	$1.80\text{E-}24 \pm 1.6\%$	1.65E-24	0.96	1.66E-24	0.96	1.59E-24	0.92	Void Box

Note: The total experimental error $(1\sigma \text{ level})$ should be calculated as the square root of the quadratic sum of the random error listed with each measurement and the systematic error indicated at the head of the column of the experimental results, as indicated on page 12 of reference /9/.

(^a) Reaction rates are in units of reactions × s⁻¹× atom⁻¹ × NESTOR Watt⁻¹.
 (^b) Experimental results contain a contribution from the NESTOR core bac

Experimental results contain a contribution from the NESTOR core background. Calculated results refer only to the neutrons produced in the fission plate per 1 Watt of NESTOR power. As indicated on page 10 of reference /9/, the E values, in the C/E ratios, are reduced by 4% in the RPV and void box and by 2% in the water gaps.



TAB. 5.2

PCA-Replica - Summary of Experimental (E) and Calculated (C) In-115(n,n') Reaction Rates^a per NESTOR Reactor Watt along the Horizontal Axis Z.

P₃-S₈ Calculations Using the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 Libraries and the Inhomogeneous Neutron Source.

Dos	Distance from Fission	Experimental Reaction Rate ^a \pm Random Error (1 σ)	BUGJEFF311.E Calculatio	BOLIB n	BUGENDF70.E Calculatio	BOLIB n	BUGLE-9 Calculatio	6 n	Reference
Pos.	Plate on the Axis Z [cm]	(E) Systematic Error ± 2.0%	Calculated Reaction Rate ^a (C)	C/E ^b	Calculated Reaction Rate ^a (C)	C/E ^b	Calculated Reaction Rate ^a (C)	C/E ^b	Location
1	1.91								
2	7.41								12 cm
3	12.41								Water Gap 1
4	14.01								
5	19.91								
6	25.41								13 cm Water Gap 2
7	30.41								
8	39.01	3.93E-24 ± 0.9%	3.89E-24	1.03	3.87E-24	1.03	3.81E-24	1.01	1/4 T RPV
9	49.61	8.23E-25 ± 1.4%	7.80E-25	0.99	7.76E-25	0.98	7.58E-25	0.96	3/4 T RPV
10	58.61	$2.31\text{E-}25 \pm 1.5\%$	2.15E-25	0.97	2.16E-25	0.97	2.09E-25	0.94	Void Box

Note: The total experimental error $(1\sigma \text{ level})$ should be calculated as the square root of the quadratic sum of the random error listed with each measurement and the systematic error indicated at the head of the column of the experimental results, as indicated on page 12 of reference /9/.

(^a) Reaction rates are in units of reactions × s⁻¹× atom⁻¹ × NESTOR Watt⁻¹.
 (^b) Experimental results contain a contribution from the NESTOR core bac

Experimental results contain a contribution from the NESTOR core background. Calculated results refer only to the neutrons produced in the fission plate per 1 Watt of NESTOR power. As indicated on page 10 of reference /9/, the E values, in the C/E ratios, are reduced by 4% in the RPV and void box.



TAB. 5.3

PCA-Replica - Summary of Experimental (E) and Calculated (C) S-32(n,p) Reaction Rates^a per NESTOR Reactor Watt along the Horizontal Axis Z.

P₃-S₈ Calculations Using the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 Libraries and the Inhomogeneous Neutron Source.

Dos	Distance from Fission	Experimental Reaction Rate ^a \pm Random Error (1 σ)	BUGJEFF311.E Calculatio	BOLIB n	BUGENDF70.F Calculatio	BOLIB n	BUGLE-9 Calculatio	6 n	Reference
Pos.	Plate on the Axis Z [cm]	(E) Systematic Error ± 4.0%	Calculated Reaction Rate ^a (C)	C/E ^b	Calculated Reaction Rate ^a (C)	C/E ^b	Calculated Reaction Rate ^a (C)	C/E ^b	Location
1	1.91								
2	7.41								12 cm
3	12.41								Water Gap 1
4	14.01								
5	19.91								
6	25.41								13 cm Water Gap 2
7	30.41								
8	39.01	1.08E-24 ± 1.5%	9.86E-25	0.95	9.78E-25	0.94	9.67E-25	0.93	1/4 T RPV
9	49.61	$1.46\text{E-}25 \pm 1.9\%$	1.38E-25	0.98	1.35E-25	0.97	1.34E-25	0.95	3/4 T RPV
10	58.61	3.73E-26 ± 1.3%	3.63E-26	1.01	3.57E-26	1.00	3.52E-26	0.98	Void Box

Note: The total experimental error $(1\sigma \text{ level})$ should be calculated as the square root of the quadratic sum of the random error listed with each measurement and the systematic error indicated at the head of the column of the experimental results, as indicated on page 12 of reference /9/.

(^a) Reaction rates are in units of reactions × s⁻¹× atom⁻¹ × NESTOR Watt⁻¹.
 (^b) Experimental results contain a contribution from the NESTOR core bac

Experimental results contain a contribution from the NESTOR core background. Calculated results refer only to the neutrons produced in the fission plate per 1 Watt of NESTOR power. As indicated on page 10 of reference /9/, the E values, in the C/E ratios, are reduced by 4% in the RPV and void box.





FIG. 5.1 PCA-Replica - Rh-103(n,n') Reaction Rate Ratios (Calculated/Experimental).



FIG. 5.2 PCA-Replica - In-115(n,n') Reaction Rate Ratios (Calculated/Experimental).



FIG. 5.3 PCA-Replica - S-32(n,p) Reaction Rate Ratios (Calculated/Experimental).



FIG. 5.4

PCA-Replica - Rh-103(n,n') Reaction Rates per Fission Plate Watt on the Horizontal Axis Z. Comparison of Experimental and Calculated Reaction Rates.





FIG. 5.5

PCA-Replica - Spatial Distribution of the Rh-103(n,n') Reaction Rates per NESTOR Watt. [reactions \times s⁻¹ \times atom⁻¹ \times NESTOR Watt⁻¹]

Horizontal Section at Y = 0.0 cm. Dosimeter Locations " \times ", 65X \times 63Y \times 182Z Spatial Meshes.





FIG. 5.6

PCA-Replica - Spatial Distribution at of the In-115(n,n') Reaction Rates per NESTOR Watt. [reactions $\times s^{-1} \times atom^{-1} \times NESTOR Watt^{-1}$]

Horizontal Section at Y = 0.0 cm. Dosimeter Locations " \times ", 65X \times 63Y \times 182Z Spatial Meshes.





FIG. 5.7

PCA-Replica - Spatial Distribution at of the S-32(n,p) Reaction Rates per NESTOR Watt. [reactions \times s⁻¹ \times atom⁻¹ \times NESTOR Watt⁻¹]

> Horizontal Section at Y = 0.0 cm. Dosimeter Locations " \times ", 65X \times 63Y \times 182Z Spatial Meshes.





FIG. 5.8

PCA-Replica - Spatial Distribution of the Neutron Fluxes per NESTOR Watt for Neutron Energy > 0.1 MeV. [neutrons \times barn⁻¹ \times s⁻¹ \times NESTOR Watt⁻¹]

> Horizontal Section at Y = 0.0 cm. Dosimeter Locations " \times ", 65X \times 63Y \times 182Z Spatial Meshes.





FIG. 5.9

PCA-Replica - Spatial Distribution of the Neutron Fluxes per NESTOR Watt for Neutron Energy > 1.0 MeV. [neutrons \times barn⁻¹ \times s⁻¹ \times NESTOR Watt⁻¹]

Horizontal Section at Y = 0.0 cm. Dosimeter Locations " \times ", 65X \times 63Y \times 182Z Spatial Meshes.





FIG. 5.10

PCA-Replica - Spatial Distribution of the Neutron Fluxes per NESTOR Watt for Neutron Energy > 3.0 MeV. [neutrons × barn⁻¹ × s⁻¹ × NESTOR Watt⁻¹]

Horizontal Section at Y = 0.0 cm. Dosimeter Locations " \times ", 65X \times 63Y \times 182Z Spatial Meshes.



TAB. 5.4

PCA-Replica - Calculated Neutron Fluxes (Φ) per NESTOR Watt in the Measure Positions along the Horizontal Axis Z for Neutron Energy (E) > 0.1, > 1.0 and > 3.0 MeV. P₃-S₈ TORT-3.2 (X,Y,Z) Calculations Using the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 Libraries and the Inhomogeneous Neutron Source.

Instant te on the Xis Z J311 $E > 0.1 \text{MeV}$ $E > 1.0 \text{MeV}$ te on the te on the Xis Z J311J311 $B70$ $B96$ J311 $B70$ Lem]J311 $B70$ $B96$ J311 $B70$ $B70$ Lual CalculationCalculationCalculationCalculation $Calculation$ $Calculation$ 1.913.39E-203.39E-20 $3.41E-20$ $1.67E-20$ $1.67E-20$ $1.67E-20$ 7.41 $6.34E-21$ $6.35E-21$ $6.35E-21$ $3.17E-21$ $3.18E-21$ 7.41 $6.34E-21$ $6.35E-21$ $6.35E-21$ $3.17E-21$ $1.06E-21$ 12.41 $2.30E-21$ $2.31E-21$ $2.30E-21$ $1.06E-21$ $1.06E-21$ 19.91 $9.03E-22$ $9.01E-22$ $8.86E-22$ $3.58E-22$ $3.56E-22$ 19.91 $9.03E-22$ $1.91E-22$ $1.91E-22$ $1.91E-22$ $1.88E-22$ $9.36E-23$ 3.041 $7.30E-23$ $7.18E-23$ $3.79E-23$ $3.80E-23$ $3.66E-23$ 3.041 $7.30E-23$ $5.10E-23$ $3.75E-23$ $3.66E-23$ $3.66E-23$ 3.041 $7.30E-23$ $5.10E-23$ $3.35E-23$ $3.79E-23$ $3.80E-23$ 44.21 $3.44E-23$ $3.39E-23$ $3.57E-24$ $7.56E-24$ 49.61 $2.04E-23$ $2.01E-23$ $1.98E-23$ $3.27E-24$ $3.31E-24$ 49.61 $2.04E-23$ $1.98E-23$ $3.27E-24$ $3.31E-24$		< NESTOR Watt ⁻¹]	Deference
J311B70B96J311B70CalculationCalculationCalculationCalculationCalculationCalculation3.39E-203.41E-201.67E-201.67E-203.39E-213.39E-213.31E-211.67E-201.67E-206.34E-216.35E-216.35E-215.35E-213.18E-2112.30E-212.31E-212.30E-211.21E-2112.30E-212.31E-212.12E-211.06E-2112.11E-212.12E-212.12E-211.06E-2119.03E-229.01E-228.86E-223.58E-2219.03E-229.01E-221.88E-229.35E-2311.91E-221.91E-221.88E-229.36E-2311.91E-221.91E-221.88E-233.79E-2311.91E-221.91E-221.88E-233.79E-2313.44E-235.05E-231.58E-231.58E-2313.44E-233.39E-233.35E-237.51E-2412.04E-232.01E-231.98E-233.27E-2412.04E-232.01E-231.98E-233.27E-24	E > 3.0	MeV	Location
1 3.39E-20 3.41E-20 1.67E-20 1.06E-21 1.06E-21 1.06E-21 1.06E-21 1.06E-21 1.06E-22 3.56E-22 3.36E-22 3.36E-22 3.36E-22 3.36E-22 3.36E-22 3.36E-22 3.36E-23 3.36E-23 3.36E-23 3.	B96 J311 B70 Leulation Calculation	B96 tion Calculation	
116.34E-216.35E-216.35E-215.17E-213.18E-21412.30E-212.31E-212.30E-211.21E-211.21E-21012.11E-212.12E-212.12E-211.06E-211.06E-21919.03E-229.01E-228.86E-223.58E-223.56E-22411.91E-221.91E-221.88E-229.36E-239.35E-23411.91E-221.91E-221.88E-229.36E-233.56E-23417.30E-237.30E-237.18E-233.79E-233.80E-23015.16E-235.10E-235.05E-231.58E-231.58E-23213.44E-233.39E-233.35E-237.51E-247.56E-24612.04E-232.01E-231.98E-233.31E-243.31E-24	.68E-20 3.79E-21 3.79E	21 3.81E-21	
412.30E-212.31E-212.30E-211.21E-211.21E-211.21E-21012.11E-212.12E-212.12E-211.06E-211.06E-21919.03E-229.01E-228.86E-223.58E-223.56E-22411.91E-221.91E-221.88E-229.36E-239.35E-23417.30E-237.30E-237.18E-239.36E-233.80E-23015.16E-237.30E-237.18E-231.58E-231.58E-23015.16E-235.05E-231.58E-231.58E-231.58E-23213.44E-233.39E-233.35E-237.51E-247.56E-24612.04E-232.01E-231.98E-233.27E-243.31E-24	.18E-21 8.13E-22 8.17E	22 8.16E-22	12 cm
01 2.11E-21 2.12E-21 2.12E-21 1.06E-21 1.06E-21 .91 9.03E-22 9.01E-22 8.86E-22 3.58E-22 3.56E-22 .41 1.91E-22 1.91E-22 1.88E-22 9.36E-23 9.35E-23 .41 7.30E-23 7.30E-23 7.18E-23 9.36E-23 9.35E-23 .01 5.16E-23 5.10E-23 7.18E-23 1.58E-23 1.58E-23 .01 5.16E-23 5.05E-23 1.58E-23 1.58E-23 .01 5.16E-23 3.35E-23 7.51E-24 7.56E-24 .61 2.04E-23 2.01E-23 1.98E-23 3.27E-24	.21E-21 3.32E-22 3.34E	22 3.33E-22	Water Gap 1
91 9.03E-22 9.01E-22 8.86E-22 3.58E-22 3.56E-22 .41 1.91E-22 1.91E-22 1.91E-22 9.36E-23 9.35E-23 .41 7.30E-23 7.30E-23 7.18E-23 9.36E-23 9.35E-23 .01 5.16E-23 5.10E-23 5.05E-23 1.58E-23 1.58E-23 .01 5.16E-23 5.10E-23 5.05E-23 1.58E-23 1.58E-23 .01 5.16E-23 5.05E-23 1.58E-23 1.58E-23 1.58E-23 .01 5.16E-23 5.05E-23 1.58E-23 1.58E-23 1.58E-23 .01 5.16E-23 3.35E-23 1.58E-23 1.58E-23 1.58E-23 .01 5.16E-23 3.35E-23 7.51E-24 7.56E-24 .61 2.04E-23 2.01E-23 1.98E-23 3.31E-24	.06E-21 2.71E-22 2.71E	22 2.70E-22	
(411.91E-221.91E-221.88E-229.36E-239.35E-23(417.30E-237.30E-237.18E-233.79E-233.80E-23(015.16E-235.10E-235.05E-231.58E-231.58E-23(015.16E-235.10E-235.05E-231.58E-231.58E-23(015.16E-233.39E-233.35E-237.51E-247.56E-24(012.04E-232.01E-231.98E-233.27E-243.31E-24	.52E-22 7.13E-23 6.99E	23 6.96E-23	
.41 7.30E-23 7.30E-23 7.18E-23 3.79E-23 3.80E-23 3.80E-24 7.56E-24 7.56E-24 7.56E-24 3.31E-24	.22E-23 2.55E-23 2.54E	23 2.51E-23	13 cm Water Gap 2
.01 5.16E-23 5.10E-23 5.05E-23 1.58E-23 1.58E-23 1.58E-23 .21 3.44E-23 3.39E-23 3.35E-23 7.51E-24 7.56E-24 .61 2.04E-23 2.01E-23 1.98E-23 3.27E-24 3.31E-24	.74E-23 1.13E-23 1.14E	23 1.12E-23	
.21 3.44E-23 3.39E-23 3.35E-23 7.51E-24 7.56E-24 .61 2.04E-23 2.01E-23 1.98E-23 3.27E-24 3.31E-24	.56E-23 3.02E-24 2.96E	24 2.93E-24	1/4 T RPV
.61 2.04E-23 2.01E-23 1.98E-23 3.27E-24 3.31E-24	.40E-24 1.16E-24 1.13E	24 1.12E-24	1/2 T RPV
	.23E-24 4.09E-25 3.94E	25 3.90E-25	3/4 T RPV
61 6.24E-24 6.17E-24 5.96E-24 8.95E-25 9.19E-25	.89E-25 1.08E-25 1.04E	25 1.03E-25	Void Box

(^a) Not included as dosimeter measure position in the PCA-Replica 12/13 Experiment.



ib.	Pag.	di
	59	118

TAB. 5.5

PCA-Replica - Calculated Neutron Flux (Φ) Ratios in the Measure Positions along the Horizontal Axis Z for Neutron Energy (E) > 0.1, > 1.0 and > 3.0 MeV. P₃-S₈ TORT-3.2 (X,Y,Z) Calculations Using the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 Libraries and the Inhomogeneous Neutron Source.

Fission Fission Axis Z [cm] 1.91 7.41 1.91 1.91 12.41 14.01 19.91 19.91 25.41 30.41	 Φ (E > 1.0 J311 Calculation 49.3 50.0 52.6 50.2) MeV) / Φ (E > B70 Calculation 49.3 50.1 52.4 50.0	0.1 MeV) B96 Calculation 49.3 50.1 52.6 50.0	Φ (E > 3.0 J311 Calculation 11.2	MeV) / Φ (E > B70 Calculation	0.1 MeV)	Φ (E > 3.0) MeV) / Φ (E >	10 MeV)	Reference
Axis Z [cm] 1.91 7.41 12.41 14.01 19.91 25.41 30.41	J311 Calculation 49.3 50.0 52.6 50.2	B70 Calculation 49.3 50.1 52.4 50.0	B96 Calculation 49.3 50.1 52.6 50.0	J311 Calculation 11.2	B70 Calculation					Location
1.91 7.41 12.41 14.01 19.91 25.41 30.41	49.3 50.0 52.6 50.2	49.3 50.1 52.4 50.0	49.3 50.1 52.6 50.0	11.2		B96 Calculation	J311 Calculation	B70 Calculation	B96 Calculation	
7.41 12.41 14.01 19.91 25.41 30.41	50.0 52.6 50.2	50.1 52.4 50.0	50.1 52.6 50.0		11.2	11.2	22.7	22.7	22.7	
12.41 14.01 19.91 25.41 30.41	52.6 50.2	52.4 50.0	52.6 50.0	12.8	12.9	12.9	25.6	25.7	25.7	12 cm
14.01 19.91 25.41 30.41	50.2	50.0	50.0	14.4	14.5	14.5	27.4	27.6	27.5	Water Gap 1
19.91 25.41 30.41				12.8	12.8	12.7	25.6	25.6	25.5	
25.41 30.41	39.6	39.5	39.7	7.9	7.8	7.9	19.9	19.6	19.8	
30.41	49.0	49.0	49.0	13.4	13.3	13.4	27.2	27.2	27.2	13 cm Water Gap 2
	51.9	52.1	52.1	15.5	15.6	15.6	29.8	30.0	29.9	I
39.01	30.6	31.0	30.9	5.9	5.8	5.8	19.1	18.7	18.8	1/4 T RPV
44.21	21.8	22.3	22.1	3.4	3.3	3.3	15.4	14.9	15.1	1/2 T RPV
49.61	16.0	16.5	16.3	2.0	2.0	2.0	12.5	11.9	12.1	3/4 T RPV
58.61	14.3	14.9	14.9	1.7	1.7	1.7	12.1	11.3	11.6	Void Box

^(a) Not included as dosimeter measure position in the PCA-Replica 12/13 Experiment.

di

118





TAB. 5.6

PCA-Replica - Summary of Experimental (E) and Calculated (C) Rh-103(n,n') Reaction Rates^a per NESTOR Reactor Watt along the Horizontal Axis Z.

P₃-S₈ TORT-3.2 (X,Y,Z) Calculations Using the BUGJEFF311.BOLIB Library and the Inhomogeneous/Homogeneous Neutron Source.

Dos. Pos	Distance from Fission Plate on	Experimental Reaction Rate ^a \pm Random Error (1 σ) (E)	BUGJEFF311.F Calculatio Inhomogene Neutron Sou	BOLIB n ous irce	BUGJEFF311.F Calculatio Homogeneo Neutron Sou	BOLIB n ous irce	Reference Location
103.	the Axis Z [cm]	Systematic Error ± 3.0%	Calculated Reaction Rate ^a (C)	ulated on Rate ^a C/E ^b Calculated Reaction Rate ^a C/E ^b (C) C/E ^b		C/E ^b	
1	1.91	$1.69\text{E-}20 \pm 3.0\%$	1.81E-20	1.09	1.74E-20	1.05	
2	7.41	3.78E-21 ± 3.0%	3.43E-21	0.93	3.30E-21	0.89	12 cm
3	12.41	$1.40\text{E-}21 \pm 3.0\%$	1.30E-21	0.95	1.26E-21	0.92	Water Gap 1
4	14.01	1.27E-21 ± 3.0%	1.15E-21	0.93	1.12E-21	0.90	
5	19.91	$4.23\text{E-}22 \pm 3.0\%$	4.18E-22	1.01	4.07E-22	0.98	
6	25.41	$1.15\text{E-}22 \pm 4.0\%$	1.02E-22	0.91	1.00E-22	0.89	13 cm Water Gap 2
7	30.41	$4.73\text{E-}23 \pm 4.0\%$	4.12E-23	0.89	4.04E-23	0.87	
8	39.01	$2.07\text{E-}23 \pm 1.0\%$	2.02E-23	1.02	1.99E-23	1.00	1/4 T RPV
9	49.61	5.53E-24 ± 1.9%	5.62E-24	1.06	5.53E-24	1.04	3/4 T RPV
10	58.61	$1.80\text{E-}24 \pm 1.6\%$	1.65E-24	0.96	1.63E-24	0.95	Void Box

Note: The total experimental error $(1\sigma \text{ level})$ should be calculated as the square root of the quadratic sum of the random error listed with each measurement and the systematic error indicated at the head of the column of the experimental results, as indicated on page 12 of reference /9/.

(a) Reaction rates are in units of reactions × s⁻¹ × atom⁻¹ × NESTOR Watt⁻¹.
 (b) Experimental results contain a contribution from the NESTOR core bac

(b) Experimental results contain a contribution from the NESTOR core background. Calculated results refer only to the neutrons produced in the fission plate per 1 Watt of NESTOR power. As indicated on page 10 of reference /9/, the E values, in the C/E ratios, are reduced by 4% in the RPV and void box and by 2% in the water gaps.



TAB. 5.7

PCA-Replica - Summary of Experimental (E) and Calculated (C) In-115(n,n') Reaction Rates^a per NESTOR Reactor Watt along the Horizontal Axis Z.

P₃-S₈ TORT-3.2 (X,Y,Z) Calculations Using the BUGJEFF311.BOLIB Library and the Inhomogeneous/Homogeneous Neutron Source.

Dos. Pos.	Distance from Fission Plate on the Axis Z [cm]	Experimental Reaction Rate ^a \pm Random Error (1 σ) (E)	BUGJEFF311.BOLIB Calculation Inhomogeneous Neutron Source		BUGJEFF311.BOLIB Calculation Homogeneous Neutron Source		Reference Location
		the AXIS Z [cm] Systematic Error $\pm 2.0\%$	Calculated Reaction Rate ^a (C)	C/E ^b	Calculated Reaction Rate ^a (C)	C/E ^b	
1	1.91						
2	7.41						12 cm
3	12.41						Water Gap 1
4	14.01						
5	19.91						
6	25.41						13 cm Water Gap 2
7	30.41						
8	39.01	$3.93\text{E-}24 \pm 0.9\%$	3.89E-24	1.03	3.82E-24	1.01	1/4 T RPV
9	49.61	8.23E-25 ± 1.4%	7.80E-25	0.99	7.68E-25	0.97	3/4 T RPV
10	58.61	$2.31\text{E-}25 \pm 1.5\%$	2.15E-25	0.97	2.12E-25	0.96	Void Box

Note: The total experimental error $(1\sigma \text{ level})$ should be calculated as the square root of the quadratic sum of the random error listed with each measurement and the systematic error indicated at the head of the column of the experimental results, as indicated on page 12 of reference /9/.

 $\begin{array}{ll} (a) & \text{Reaction rates are in units of reactions} \times s^{-1} \times atom^{-1} \times NESTOR \ Watt^{-1}. \\ (b) & \text{Experimental results contain a contribution from the NESTOR core back and the set of t$

(^b) Experimental results contain a contribution from the NESTOR core background. Calculated results refer only to the neutrons produced in the fission plate per 1 Watt of NESTOR power. As indicated on page 10 of reference /9/, the E values, in the C/E ratios, are reduced by 4% in the RPV and void box.



TAB. 5.8

PCA-Replica - Summary of Experimental (E) and Calculated (C) S-32(n,p) Reaction Rates^a per NESTOR Reactor Watt along the Horizontal Axis Z.

P₃-S₈ TORT-3.2 (X,Y,Z) Calculations Using the BUGJEFF311.BOLIB Library and the Inhomogeneous/Homogeneous Neutron Source.

Dos. Pos.	Distance from Fission Plate on	Experimental Reaction Rate ^a \pm Random Error (1 σ) (E)	BUGJEFF311.BOLIB Calculation Inhomogeneous Neutron Source		BUGJEFF311.BOLIB Calculation Homogeneous Neutron Source		Reference Location
	[cm]	Systematic Error ± 4.0%	Calculated Reaction Rate ^a (C)	C/E ^b	Calculated Reaction Rate ^a (C)	C/E ^b	
1	1.91						
2	7.41						12 cm
3	12.41						Water Gap 1
4	14.01						
5	19.91						
6	25.41						13 cm Water Gap 2
7	30.41						
8	39.01	$1.08\text{E-}24 \pm 1.5\%$	9.86E-25	0.95	9.67E-25	0.93	1/4 T RPV
9	49.61	$1.46\text{E-}25 \pm 1.9\%$	1.38E-25	0.98	1.35E-25	0.97	3/4 T RPV
10	58.61	$3.73\text{E-}26 \pm 1.3\%$	3.63E-26	1.01	3.58E-26	1.00	Void Box

Note: The total experimental error $(1\sigma \text{ level})$ should be calculated as the square root of the quadratic sum of the random error listed with each measurement and the systematic error indicated at the head of the column of the experimental results, as indicated on page 12 of reference /9/.

 $\begin{array}{ll} (a) & \text{Reaction rates are in units of reactions} \times s^{-1} \times atom^{-1} \times NESTOR \ Watt^{-1}. \\ (b) & \text{Experimental results contain a contribution from the NESTOR core back and the set of t$

(^b) Experimental results contain a contribution from the NESTOR core background. Calculated results refer only to the neutrons produced in the fission plate per 1 Watt of NESTOR power. As indicated on page 10 of reference /9/, the E values, in the C/E ratios, are reduced by 4% in the RPV and void box.





FIG. 5.11 PCA-Replica - Rh-103(n,n') Reaction Rate Ratios (Calculated/Experimental).



FIG. 5.12 PCA-Replica - In-115(n,n') Reaction Rate Ratios (Calculated/Experimental).



FIG. 5.13 PCA-Replica - S-32(n,p) Reaction Rate Ratios (Calculated/Experimental).

		Sigla di identificazione	Rev.	Distrib.	Pag.	di
ENEA	Ricerca Sistema Elettrico	ADPFISS-LP1-024	0	L	65	118



FIG. 5.14

PCA-Replica - Rh-103(n,n') Reaction Rate Ratios (Calculated/Experimental) vs. Different S_N Approximations in P₃Calculations.



FIG. 5.15

PCA-Replica - Rh-103(n,n') Reaction Rate Ratios (Calculated/Experimental) vs. Different S_N Approximations in P₅ Calculations.

		Sigla di identificazione	Rev.	Distrib.	Pag.	di
ENEN	Ricerca Sistema Elettrico	ADPFISS-LP1-024	0	L	66	118



FIG. 5.16

PCA-Replica - In-115(n,n') Reaction Rate Ratios (Calculated/Experimental) vs. Different S_N Approximations in P₃ Calculations.



FIG. 5.17

PCA-Replica - In-115(n,n') Reaction Rate Ratios (Calculated/Experimental) vs. Different S_N Approximations in P₅ Calculations.

		Sigla di identificazione	Rev.	Distrib.	Pag.	di
ENEA	Ricerca Sistema Elettrico	ADPFISS-LP1-024	0	L	67	118



FIG. 5.18

 $\label{eq:pca-Replica-S-32(n,p)} \begin{array}{l} \mbox{Reaction Rate Ratios (Calculated/Experimental)} \\ \mbox{vs. Different S_N Approximations in P_3 Calculations.} \end{array}$



FIG. 5.19

PCA-Replica - S-32(n,p) Reaction Rate Ratios (Calculated/Experimental) vs. Different S_N Approximations in P₅ Calculations.



5.2 - Spectral Results

The spectral measures (see 2.3) in the PCA-Replica 12/13 experiment were performed in two positions (see FIG. 2.3): 1/4 T RPV and void box. Two kinds of spectrometer were used (see 2.3). The spherical hydrogen-filled proportional counters of type SP-2 were used in combination, to cover the energy range from 50.0 keV to 1.2 MeV. The neutron fluxes between 1.0 and 10.0 MeV were determined with a spherical 3.5 ml organic liquid (NE213) scintillator.

The neutron spectra calculated in the 1/4 T RPV measure position with the three libraries BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 are shown in FIG. 5.1 and are compared with the corresponding experimental neutron spectrum. The calculated neutron spectra in the 1/4 T RPV measure position obtained using BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 are singularly compared with the corresponding experimental neutron spectrum, respectively in the FIGs. 5.2, 5.3 and 5.4.

The neutron spectra calculated in the void box measure position using the three libraries BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 are shown in FIG. 5.5 and are compared with the corresponding experimental neutron spectrum. The calculated neutron spectra in the void box measure position obtained with BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 are singularly compared with the corresponding experimental neutron spectrum, respectively in the FIGs. 5.6, 5.7 and 5.8. The group values of the experimental neutron spectra in both measure positions were taken from the corresponding "as measured" data reported in TAB. 2.5, reduced by 4% to eliminate (see 2.3) the contribution from the NESTOR core neutron leakage background. The neutron group structure of the BUGLE-96 library with the energy limits in MeV is reported in TAB. 5.9 to make easier the comparison of the energy limits in MeV of the experimental neutron group structure reported in TAB. 2.5 with the neutron group structure used in the calculations.

A comparison of the calculated neutron spectra obtained using the BUGJEFF311.BOLIB library is reported in FIG. 5.9 (see for comparison the FIG. 7 of reference /9/) in water, mild steel and air, in the measure positions No. 7, 8, 9 and 10 along the horizontal axis Z (see for example TAB. 5.1 for the dosimeter measure position number and the relative distance from the fission plate).

The fast neutron spectra calculated in the ten measure positions (see 5.1) plus the additional one at 1/2 T RPV are reported in the Appendixes A (see TABs. A1÷A11), B (see TABs. B1÷B11) and C (see TABs. C1÷C11), referring respectively to the calculations using the three libraries BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96.

All the calculated spectral results reported in the previously cited figures and tables are represented with the normalization per 1 fission plate Watt and were obtained with the three libraries BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 and the TORT-3.2 code in P₃-S₈ approximation using the inhomogeneous neutron source.



FIG. 5.1

PCA-Replica - Comparison of Experimental and Calculated Neutron Spectra in Mild Steel, in the 1/4 T RPV Measure Position No. 8 at Z = 39.01 cm.

P₃-S₈ TORT-3.2 (X,Y,Z) Calculations Using the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 Libraries and the Inhomogeneous Neutron Source.





FIG. 5.2

PCA-Replica - Comparison of Experimental and Calculated Neutron Spectra in Mild Steel, in the 1/4 T RPV Measure Position No. 8 at Z = 39.01 cm.




FIG. 5.3







FIG. 5.4

PCA-Replica - Comparison of Experimental and Calculated Neutron Spectra in Mild Steel, in the 1/4 T RPV Measure Position No. 8 at Z = 39.01 cm.





FIG. 5.5

PCA-Replica - Comparison of Experimental and Calculated Neutron Spectra in Air, in the Void Box Measure Position No. 10 at Z = 58.61 cm.

P₃-S₈ TORT-3.2 (X,Y,Z) Calculations Using the BUGJEFF311.BOLIB, BUGENDF70.BOLIB and BUGLE-96 Libraries and the Inhomogeneous Neutron Source.





FIG. 5.6

PCA-Replica - Comparison of Experimental and Calculated Neutron Spectra in Air, in the Void Box Measure Position No. 10 at Z = 58.61 cm.





FIG. 5.7

PCA-Replica - Comparison of Experimental and Calculated Neutron Spectra in Air, in the Void Box Measure Position No. 10 at Z = 58.61 cm.





FIG. 5.8







FIG. 5.9

PCA-Replica - Comparison of Calculated Neutron Spectra in Water, Mild Steel and Air, in the Measure Positions No. 7, 8, 9 and 10 along the Horizontal Axis Z.







TAB. 5.9

Neutron Group Energy Boundaries, Energy Widths and Lethargy Widths for the BUGLE-96 Library.

Broad Group	Upper Energy[MeV]	Energy Width[MeV]	Lethargy Width
1	1.7332E+01	3.1410E+00	1.9995E-01
2	1.4191E+01	1.9770E+00	1.5002E-01
3	1.2214E+01	2.2140E+00	2.0000E-01
4	1.0000E+01	1.3929E+00	1.5000E-01
5	8.6071E+00	1.1989E+00	1.5000E-01
6	7.4082E+00	1.3429E+00	2.0000E-01
7	6.0653E+00	1.0994E+00	1.9999E-01
8	4.9659E+00	1.2871E+00	3.0001E-01
9	3.6788E+00	6.6690E-01	2.0002E-01
10	3.0119E+00	2.8660E-01	9.9993E-02
11	2.7253E+00	2.5930E-01	9.9981E-02
12	2.4660E+00	1.0070E-01	4.1693E-02
13	2.3653E+00	1.9600E-02	8.3210E-03
14	2.3457E+00	1.1440E-01	4.9999E-02
15	2.2313E+00	3.1080E-01	1.5000E-01
16	1.9205E+00	2.6750E-01	1.4999E-01
17	1.6530E+00	2.9960E-01	1.9997E-01
18	1.3534E+00	3.5080E-01	3.0002E-01
19	1.0026E+00	1.8175E-01	2.0001E-01
20	8.2085E-01	7.8110E-02	9.9994E-02
21	7.4274E-01	1.3464E-01	2.0001E-01
22	6.0810E-01	1.1023E-01	2.0000E-01
23	4.9787E-01	1.2904E-01	3.0000E-01
24	3.6883E-01	7.1620E-02	2.1590E-01
25	2.9721E-01	1.1405E-01	4.8408E-01
26	1.8316E-01	7.2070E-02	5.0002E-01
27	1.1109E-01	4.3711E-02	5.0001E-01
28	6.7379E-02	2.6511E-02	4.9999E-01
29	4.0868E-02	9.0400E-03	2.5000E-01
30	3.1828E-02	5.7700E-03	2.0002E-01
31	2.6058E-02	1.8820E-03	7.4964E-02
32	2.4176E-02	2.3010E-03	1.0002E-01
33	2.1875E-02	6.8410E-03	3.7503E-01
34	1.5034E-02	7.9323E-03	7.4998E-01
35	7.1017E-03	3.7471E-03	7.5000E-01
36	3.3546E-03	1.7700E-03	7.5000E-01
37	1.5846E-03	1.1306E-03	1.2500E+00
38	4.5400E-04	2.3955E-04	7.5002E-01
39	2.1445E-04	1.1315E-04	7.4999E-01
40	1.0130E-04	6.4034E-05	1.0000E+00
41	3.7266E-05	2.6589E-05	1.2500E+00
42	1.0677E-05	5.6335E-06	7.4999E-01
43	5.0435E-06	3.1881E-06	1.0000E+00
44	1.8554E-06	9.7897E-07	7.5000E-01
45	8.7643E-07	4.6244E-07	7.5002E-01
46	4.1399E-07	3.1399E-07	1.4207E+00
47	1.0000E-07	9.9990E-08	9.2103E+00
	1.0000E-11		



6 - CONCLUSION

The PCA-Replica 12/13 water/iron (H₂O/Fe) engineering neutron shielding benchmark experiment was analyzed through three-dimensional (3D) fixed source transport calculations in Cartesian (X, Y, Z) geometry performed with the ORNL TORT-3.2 discrete ordinates (S_N) code. Three similar broad-group coupled neutron/photon working cross section libraries with the same (47 n + 20 γ) energy group structure and the same FIDO-ANISN format were used in the transport calculations to obtain neutron dose and neutron spectrum calculated results. ENEA-Bologna BUGJEFF311.BOLIB (JEFF-3.1.1 In particular the data) and (ENDF/B-VII.0 data) libraries and BUGENDF70.BOLIB the ORNL BUGLE-96 (ENDF/B-VI.3 data) library, specifically conceived for LWR shielding and pressure vessel dosimetry applications, were alternatively employed in the transport calculations.

Processed cross section sets of three (Rh-103(n,n')Rh-103m, In-115(n,n')In-115m and S-32(n,p)P-32) threshold activation dosimeters, derived from the IAEA IRDF-2002 dosimetry file, were used to obtain the calculated dosimeter reaction rates.

The reference dosimetric and spectral results were obtained with transport calculations in the P_3 - S_8 approximation using the experimental inhomogeneous fission neutron source generated in the PCA-Replica fission plate.

Almost all the reaction rate calculated results obtained with the three previously cited libraries present deviations from the corresponding experimental results within $\pm 10\%$.

The calculated reaction rates obtained with a simplified homogeneous fission neutron source give results sistematically underestimated of few percents with respect to the corresponding ones obtained with the inhomogeneous fission neutron source.

A parametric research on the P_N - S_N orders of approximation in the transport calculations up to the P_5 - S_{16} approximation demonstrated that a good stabilization of the calculated results is already obtained through the P_3 - S_8 approximation, commonly used in the LWR shielding and neutron damage analyses.



REFERENCES

- /1/ W.W. Engle, Jr., A Users Manual for ANISN, A One Dimensional Discrete Ordinates Transport Code with Anisotropic Scattering, ORNL K-1693, Updated June 6, 1973. Available from OECD-NEA Data Bank as CCC-254 ANISN-ORNL.
- M. Pescarini, V. Sinitsa, R. Orsi, M. Frisoni, BUGJEFF311.BOLIB A JEFF-3.1.1 Broad-Group Coupled (47 n + 20 γ) Cross Section Library in FIDO-ANISN Format for LWR Shielding and Pressure Vessel Dosimetry Applications, ENEA-Bologna Technical Report UTFISSM-P9H6-002, May 12, 2011. ENEA-Bologna Technical Report UTFISSM-P9H6-002 Revision 1 published on March 14, 2013. Available from OECD-NEA Data Bank as NEA-1866/01 ZZ BUGJEFF311.BOLIB.
- /3/ M. Pescarini, V. Sinitsa, R. Orsi, M. Frisoni, BUGENDF70.BOLIB An ENDF/B-VII.0 Broad-Group Coupled (47 n + 20 γ) Cross Section Library in FIDO-ANISN Format for LWR Shielding and Pressure Vessel Dosimetry Applications, ENEA-Bologna Technical Report UTFISSM-P9H6-008, January 1, 2013. Available from OECD-NEA Data Bank as NEA-1872/01 ZZ BUGENDF70.BOLIB.
- /4/ The JEFF-3.1.1 Nuclear Data Library, JEFF Report 22, OECD-NEA Data Bank, 2009.
- /5/ The JEFF-3.1 Nuclear Data Library, JEFF Report 21, OECD-NEA Data Bank, 2006.
- /6/ M.B. Chadwick et al., ENDF/B-VII.0: Next Generation Evaluated Nuclear Data Library for Nuclear Science and Technology, Nuclear Data Sheets, Volume 107, Number 12, pp. 2931-3060, December 2006.
- /7/ J.E. White, D.T. Ingersoll, R.Q. Wright, H.T. Hunter, C.O. Slater, N.M. Greene, R.E. MacFarlane, R.W. Roussin, Production and Testing of the Revised VITAMIN-B6 Fine-Group and the BUGLE-96 Broad-Group Neutron/Photon Cross-Section Libraries Derived from ENDF/B-VI.3 Nuclear Data, Oak Ridge, ORNL Report ORNL-6795/R1, NUREG/CR-6214, Revision 1, January 1995. VITAMIN-B6 library available from OECD-NEA Data Bank as DLC-0184 ZZ VITAMIN-B6. BUGLE-96 library available from OECD-NEA Data Bank as DLC-0185 ZZ BUGLE-96.
- /8/ P.F. Rose, ENDF/B-VI Summary Documentation, Brookhaven National Laboratory, BNL-NCS-17541 (ENDF-201) 4th Edition, October 1991.
- /9/ J. Butler, M.D. Carter, I.J. Curl, M.R. March, A.K. McCracken, M.F. Murphy, A. Packwood, The PCA-Replica Experiment Part I Winfrith Measurements and Calculations, UKAEA, AEE Winfrith Report AEEW-R 1736, January 1984.
- /10/ J. Butler, The NESTOR Shielding and Dosimetry Improvement Programme NESDIP for PWR Applications, PRPWG/P (82)5, Internal UKAEA Document, November 1982.
- /11/ Radiation Shielding Integral Benchmark Archive Database (SINBAD), OECD-NEA Data Bank/ ORNL-RSICC, SINBAD REACTOR, NEA-1517, 2009 Edition.
- /12/ I. Kodeli, E. Sartori, B. Kirk, SINBAD Shielding Benchmark Experiments Status and Planned Activities, The American Society's 14th Biennial Topical Meeting of the Radiation Protection and Shielding Division, Carlsbad, New Mexico, USA, April 3-6, 2006.



- /13/ W.A. Rhoades, D.B. Simpson, The TORT Three-Dimensional Discrete Ordinates Neutron/Photon Transport Code (TORT Version 3), Oak Ridge, ORNL Report ORNL/TM-13221, October 1997.
- /14/ DOORS3.1 One-, Two- and Three-Dimensional Discrete Ordinates Neutron/Photon Transport Code System, ORNL, RSIC Computer Code Collection CCC-650, August 1996. Available from OECD-NEA Data Bank as CCC-0650/04 DOORS-3.2A.
- /15/ R. Orsi, M. Pescarini, V. Sinitsa, IRDF-2002 Dosimetry Cross Section Processing in the BUGLE-96 (47 n) Neutron Group Structure Using Flat and Updated Problem Dependent Neutron Spectra, ENEA-Bologna Technical Report UTFISSM-P9H6-006, May 9, 2012.
- /16/ O.Bersillon, L.R. Greenwood, P.J. Griffin, W. Mannhart, H.J. Nolthenius, R. Paviotti-Corcuera, K.I. Zolotarev, E.M. Zsolnay, International Reactor Dosimetry File 2002 (IRDF-2002), IAEA, Vienna, Austria, Technical Reports Series No. 452, 2006.
- /17/ R. Orsi, ADEFTA Version 4.1: A Program to Calculate the Atomic Densities of a Compositional Model for Transport Analysis, ENEA-Bologna Technical Report FPN-P9H6-010, May 20, 2008. Available from OECD-NEA Data Bank as NEA-1708/06 ADEFTA 4.1.
- /18/ R. Orsi, BOT3P Version 5.3: A Pre/Post-Processor System for Transport Analysis, ENEA-Bologna Technical Report FPN-P9H6-011, October 22, 2008. Available from OECD-NEA Data Bank as NEA-1678/09 BOT3P-5.3.
- /19/ R. Orsi, The ENEA-Bologna pre-post-Processor Package BOT3P for the DORT and TORT Transport Codes (Version 1.0 - December 1999), JEF/DOC-828, JEFF Working Group Meeting on Benchmark Testing, Data Processing and Evaluations, OECD-NEA Data Bank, Issy-les-Moulineaux, France, May 22-24, 2000.
- /20/ R. Orsi, BOT3P: Bologna Transport Analysis Pre-Post-Processors Version 1.0, Nuclear Science and Engineering, Technical Note, Volume 142, pp. 349-354, 2002.
- /21/ R. Orsi, BOT3P: Bologna Transport Analysis Pre-Post-Processors Version 3.0, Nuclear Science and Engineering, Technical Note, Volume 146, pp. 248-255, 2004.
- /22/ W. N. McElroy Editor, LWR Pressure Vessel Surveillance Dosimetry Improvement Program: PCA Experiments and Blind Tests, HEDL-TME 80-87, NUREG/CR-1861, 1981.
- /23/ P. C. Miller, A Review of LWR pressure Vessel Dosimetry and Associated Shielding Studies, Proceedings of the UKAEA/OECD-NEA 7th International Conference on Radiation Shielding, Bournemouth, United Kingdom, September 12-16, 1988, Vol. 1, pp. 33-47.
- /24/ J.H. Baard, W.L. Zijp, H.J. Nolthenius, Nuclear Data Guide for Reactor Neutron Metrology, Kluwer Academic Publishers, 1989.
- /25/ G. Hehn, A. Sohn, M. Mattes, G. Pfister, IKE Calculations of the OECD-NEA Benchmarks VENUS-1 and VENUS-3 for Computing Radiation Dose to Reactor



Pressure Vessel and Internals, Universität Stuttgart, Institut für Kernenergetik und Energiesysteme, IKE 6 NEA 2, December 1997.

- M. Pescarini, V. Sinitsa, R. Orsi, VITJEFF311.BOLIB A JEFF-3.1.1 Multi-Group Coupled (199 n + 42 γ) Cross Section Library in AMPX Format for Nuclear Fission Applications, ENEA-Bologna Technical Report UTFISSM-P9H6-003, November 10, 2011. ENEA-Bologna Technical Report UTFISSM-P9H6-003 Revision 1 published on March 14, 2013. Available from OECD-NEA Data Bank as NEA-1869/01 ZZ VITJEFF311.BOLIB.
- /27/ I.I. Bondarenko, M.N. Nikolaev, L.P. Abagyan, N.O. Bazaziants, Group Constants for Nuclear Reactors Calculations, Consultants Bureau, New York, 1964.
- /28/ V. Sinitsa, M. Pescarini, ENEA-Bologna 2007 Revision of the SCAMPI (ORNL) Nuclear Data Processing System, ENEA-Bologna Technical Report FPN-P9H6-006, September 13, 2007.
- /29/ SCAMPI Collection of Codes for Manipulating Multigroup Cross Section Libraries in AMPX Format, ORNL, RSIC Peripheral Shielding Routine Collection PSR-352, September 1995. Available from OECD-NEA Data Bank as PSR-0352/05 SCAMPI, version of the ORNL SCAMPI system corresponding to the last ENEA-Bologna 2007 Revision (see /27/).
- /30/ M. Pescarini, V. Sinitsa, R. Orsi, M. Frisoni, VITENDF70.BOLIB An ENDF/B-VII.0 Multi-Group Coupled (199 n + 42 γ) Cross Section Library in AMPX Format for Nuclear Fission Applications, ENEA-Bologna Technical Report UTFISSM-P9H6-005, May 25, 2012. Available from OECD-NEA Data Bank as NEA-1870/01 ZZ VITENDF70.BOLIB.
- /31/ American National Standard, American Nuclear Society, Neutron and Gamma-Ray Cross Sections for Nuclear Radiation Protection Calculations for Nuclear Power Plants, ANSI/ANS-6.1.2-1999 (R2009).
- /32/ D.E. Cullen, PREPRO 2007: 2007 ENDF/B Pre-processing Codes (ENDF/B-VII Tested), LLNL, owned, maintained and distributed by IAEA-NDS, Vienna, Austria, IAEA Report IAEA-NDS-39, Rev. 13, March 17, 2007. Available from OECD-NEA Data Bank as IAEA-1379 PREPRO-2007.
- /33/ J.K. Tuli, Nuclear Wallet Cards (6th Edition), National Nuclear Data Centre, Brookhaven National Laboratory, Upton, New York 11973-5000, USA, January 2000.
- /34/ M. Pescarini, DOT 3.5-E (DOT-3.5-E/JEF-1) Analysis of the PCA-Replica (H₂O/Fe) Shielding Benchmark for the LWR-PV Damage Prediction, ENEA Technical Report RT/INN/90/21, October 1990.



di

APPENDIX A

Neutron Spectra Calculated along the Horizontal Axis Z Using BUGJEFF311.BOLIB



TAB. A1

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 1 Measure Position No. 1 at Z = 1.91 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGJEFF311.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.1745E+03	1.1745E+03
2	1.4191E+01	4.7265E+03	5.9010E+03
3	1.2214E+01	2.7126E+04	3.3027E+04
4	1.0000E+01	5.9906E+04	9.2933E+04
5	8.6071E+00	1.3367E+05	2.2661E+05
6	7.4082E+00	3.7662E+05	6.0322E+05
7	6.0653E+00	7.5424E+05	1.3575E+06
8	4.9659E+00	2.1614E+06	3.5189E+06
9	3.6788E+00	2.0502E+06	5.5690E+06
10	3.0119E+00	1.2840E+06	6.8530E+06
11	2.7253E+00	1.4474E+06	8.3004E+06
12	2.4660E+00	7.9273E+05	9.0931E+06
13	2.3653E+00	1.3839E+05	9.2315E+06
14	2.3457E+00	8.0801E+05	1.0040E+07
15	2.2313E+00	2.5496E+06	1.2589E+07
16	1.9205E+00	2.6893E+06	1.5278E+07
17	1.6530E+00	3.6930E+06	1.8971E+07
18	1.3534E+00	5.8291E+06	2.4800E+07
19	1.0026E+00	3.0328E+06	2.7833E+07
20	8.2085E-01	1.7216E+06	2.9555E+07
21	7.4274E-01	3.1970E+06	3.2752E+07
22	6.0810E-01	2.9181E+06	3.5670E+07
23	4.9787E-01	3.8690E+06	3.9539E+07
24	3.6883E-01	2.3300E+06	4.1869E+07
25	2.9721E-01	4.5969E+06	4.6466E+07
26	1.8316E-01	3.1870E+06	4.9653E+07
27	1.1109E-01	2.8765E+06	5.2529E+07
28	6.7379E-02	2.1955E+06	5.4725E+07
29	4.0868E-02	6.5630E+05	5.5381E+07
	3.1828E-02		



TAB. A2

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 1 Measure Position No. 2 at Z = 7.41 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGJEFF311.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	3.2155E+02	3.2155E+02
2	1.4191E+01	1.2471E+03	1.5687E+03
3	1.2214E+01	6.7186E+03	8.2873E+03
4	1.0000E+01	1.4531E+04	2.2819E+04
5	8.6071E+00	3.1418E+04	5.4237E+04
6	7.4082E+00	9.0598E+04	1.4483E+05
7	6.0653E+00	1.7537E+05	3.2020E+05
8	4.9659E+00	4.7137E+05	7.9158E+05
9	3.6788E+00	4.0374E+05	1.1953E+06
10	3.0119E+00	2.7266E+05	1.4680E+06
11	2.7253E+00	3.1969E+05	1.7877E+06
12	2.4660E+00	1.6103E+05	1.9487E+06
13	2.3653E+00	3.3069E+04	1.9818E+06
14	2.3457E+00	1.7971E+05	2.1615E+06
15	2.2313E+00	4.9687E+05	2.6583E+06
16	1.9205E+00	4.8776E+05	3.1461E+06
17	1.6530E+00	6.5372E+05	3.7998E+06
18	1.3534E+00	8.9748E+05	4.6973E+06
19	1.0026E+00	5.4132E+05	5.2386E+06
20	8.2085E-01	3.1837E+05	5.5570E+06
21	7.4274E-01	5.5720E+05	6.1142E+06
22	6.0810E-01	5.1658E+05	6.6308E+06
23	4.9787E-01	6.0756E+05	7.2383E+06
24	3.6883E-01	4.4534E+05	7.6837E+06
25	2.9721E-01	8.6919E+05	8.5529E+06
26	1.8316E-01	7.1702E+05	9.2699E+06
27	1.1109E-01	6.2031E+05	9.8902E+06
28	6.7379E-02	5.4797E+05	1.0438E+07
29	4.0868E-02	2.5839E+05	1.0697E+07
	3.1828E-02		
1			



TAB. A3

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 1 Measure Position No. 3 at Z = 12.41 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGJEFF311.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.7534E+02	1.7534E+02
2	1.4191E+01	6.6115E+02	8.3649E+02
3	1.2214E+01	3.4131E+03	4.2496E+03
4	1.0000E+01	7.2340E+03	1.1484E+04
5	8.6071E+00	1.5027E+04	2.6511E+04
6	7.4082E+00	4.2573E+04	6.9084E+04
7	6.0653E+00	7.7191E+04	1.4627E+05
8	4.9659E+00	1.9103E+05	3.3730E+05
9	3.6788E+00	1.5158E+05	4.8888E+05
10	3.0119E+00	1.0573E+05	5.9462E+05
11	2.7253E+00	1.2282E+05	7.1744E+05
12	2.4660E+00	6.2542E+04	7.7998E+05
13	2.3653E+00	1.3644E+04	7.9362E+05
14	2.3457E+00	7.1706E+04	8.6533E+05
15	2.2313E+00	1.8755E+05	1.0529E+06
16	1.9205E+00	1.8034E+05	1.2332E+06
17	1.6530E+00	2.3843E+05	1.4716E+06
18	1.3534E+00	3.1567E+05	1.7873E+06
19	1.0026E+00	1.9109E+05	1.9784E+06
20	8.2085E-01	1.1091E+05	2.0893E+06
21	7.4274E-01	1.9720E+05	2.2865E+06
22	6.0810E-01	1.8141E+05	2.4679E+06
23	4.9787E-01	2.0898E+05	2.6769E+06
24	3.6883E-01	1.5334E+05	2.8302E+06
25	2.9721E-01	2.9453E+05	3.1248E+06
26	1.8316E-01	2.4157E+05	3.3663E+06
27	1.1109E-01	2.0941E+05	3.5758E+06
28	6.7379E-02	1.8385E+05	3.7596E+06
29	4.0868E-02	8.7332E+04	3.8469E+06
	3.1828E-02		



TAB. A4

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 1 Measure Position No. 4 at Z = 14.01 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGJEFF311.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.4738E+02	1.4738E+02
2	1.4191E+01	5.5198E+02	6.9936E+02
3	1.2214E+01	2.8214E+03	3.5208E+03
4	1.0000E+01	5.9519E+03	9.4727E+03
5	8.6071E+00	1.2275E+04	2.1748E+04
6	7.4082E+00	3.4855E+04	5.6603E+04
7	6.0653E+00	6.2805E+04	1.1941E+05
8	4.9659E+00	1.5491E+05	2.7431E+05
9	3.6788E+00	1.2384E+05	3.9816E+05
10	3.0119E+00	8.7762E+04	4.8592E+05
11	2.7253E+00	1.0143E+05	5.8735E+05
12	2.4660E+00	5.2536E+04	6.3988E+05
13	2.3653E+00	1.1523E+04	6.5141E+05
14	2.3457E+00	6.1709E+04	7.1312E+05
15	2.2313E+00	1.6549E+05	8.7860E+05
16	1.9205E+00	1.6240E+05	1.0410E+06
17	1.6530E+00	2.2002E+05	1.2610E+06
18	1.3534E+00	3.0658E+05	1.5676E+06
19	1.0026E+00	1.8119E+05	1.7488E+06
20	8.2085E-01	1.0053E+05	1.8493E+06
21	7.4274E-01	2.0310E+05	2.0524E+06
22	6.0810E-01	1.8048E+05	2.2329E+06
23	4.9787E-01	2.0773E+05	2.4406E+06
24	3.6883E-01	1.5446E+05	2.5951E+06
25	2.9721E-01	2.6752E+05	2.8626E+06
26	1.8316E-01	2.3188E+05	3.0945E+06
27	1.1109E-01	1.7876E+05	3.2733E+06
28	6.7379E-02	1.6408E+05	3.4373E+06
29	4.0868E-02	6.9564E+04	3.5069E+06
	3.1828E-02		



TAB. A5

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 2 Measure Position No. 5 at Z = 19.91 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGJEFF311.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	3.9236E+01	3.9236E+01
2	1.4191E+01	1.4449E+02	1.8373E+02
3	1.2214E+01	7.4182E+02	9.2554E+02
4	1.0000E+01	1.5631E+03	2.4887E+03
5	8.6071E+00	3.1775E+03	5.6662E+03
6	7.4082E+00	8.6142E+03	1.4280E+04
7	6.0653E+00	1.5373E+04	2.9653E+04
8	4.9659E+00	4.0062E+04	6.9715E+04
9	3.6788E+00	3.5118E+04	1.0483E+05
10	3.0119E+00	2.4819E+04	1.2965E+05
11	2.7253E+00	2.9183E+04	1.5883E+05
12	2.4660E+00	1.4619E+04	1.7345E+05
13	2.3653E+00	3.6598E+03	1.7711E+05
14	2.3457E+00	1.8755E+04	1.9587E+05
15	2.2313E+00	5.2799E+04	2.4867E+05
16	1.9205E+00	5.7975E+04	3.0664E+05
17	1.6530E+00	8.4440E+04	3.9108E+05
18	1.3534E+00	1.3844E+05	5.2953E+05
19	1.0026E+00	9.5495E+04	6.2502E+05
20	8.2085E-01	4.7421E+04	6.7244E+05
21	7.4274E-01	1.1265E+05	7.8509E+05
22	6.0810E-01	9.6260E+04	8.8135E+05
23	4.9787E-01	1.0310E+05	9.8444E+05
24	3.6883E-01	9.1617E+04	1.0761E+06
25	2.9721E-01	1.3288E+05	1.2089E+06
26	1.8316E-01	1.1464E+05	1.3236E+06
27	1.1109E-01	7.7971E+04	1.4015E+06
28	6.7379E-02	7.1154E+04	1.4727E+06
29	4.0868E-02 3.1828E-02	2.7027E+04	1.4997E+06



TAB. A6

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 2 Measure Position No. 6 at Z = 25.41 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGJEFF311.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.8666E+01	1.8666E+01
2	1.4191E+01	6.7289E+01	8.5955E+01
3	1.2214E+01	3.2948E+02	4.1543E+02
4	1.0000E+01	6.7552E+02	1.0910E+03
5	8.6071E+00	1.3263E+03	2.4172E+03
6	7.4082E+00	3.5474E+03	5.9647E+03
7	6.0653E+00	6.0355E+03	1.2000E+04
8	4.9659E+00	1.4332E+04	2.6333E+04
9	3.6788E+00	1.1166E+04	3.7499E+04
10	3.0119E+00	7.7652E+03	4.5264E+04
11	2.7253E+00	8.9677E+03	5.4231E+04
12	2.4660E+00	4.4839E+03	5.8715E+04
13	2.3653E+00	1.1244E+03	5.9840E+04
14	2.3457E+00	5.5027E+03	6.5342E+04
15	2.2313E+00	1.4102E+04	7.9444E+04
16	1.9205E+00	1.4145E+04	9.3589E+04
17	1.6530E+00	1.9072E+04	1.1266E+05
18	1.3534E+00	2.6043E+04	1.3870E+05
19	1.0026E+00	1.6428E+04	1.5513E+05
20	8.2085E-01	9.4910E+03	1.6462E+05
21	7.4274E-01	1.7412E+04	1.8204E+05
22	6.0810E-01	1.6136E+04	1.9817E+05
23	4.9787E-01	1.8555E+04	2.1673E+05
24	3.6883E-01	1.3705E+04	2.3043E+05
25	2.9721E-01	2.6594E+04	2.5703E+05
26	1.8316E-01	2.1902E+04	2.7893E+05
27	1.1109E-01	1.8909E+04	2.9784E+05
28	6.7379E-02	1.6683E+04	3.1452E+05
29	4.0868E-02	7.8666E+03	3.2239E+05
	3.1828E-02		



TAB. A7

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 2 Measure Position No. 7 at Z = 30.41 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGJEFF311.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.0523E+01	1.0523E+01
2	1.4191E+01	3.6720E+01	4.7243E+01
3	1.2214E+01	1.7086E+02	2.1810E+02
4	1.0000E+01	3.4121E+02	5.5931E+02
5	8.6071E+00	6.4783E+02	1.2071E+03
6	7.4082E+00	1.7140E+03	2.9211E+03
7	6.0653E+00	2.8123E+03	5.7334E+03
8	4.9659E+00	6.3081E+03	1.2042E+04
9	3.6788E+00	4.6496E+03	1.6691E+04
10	3.0119E+00	3.2186E+03	1.9910E+04
11	2.7253E+00	3.6712E+03	2.3581E+04
12	2.4660E+00	1.8532E+03	2.5434E+04
13	2.3653E+00	4.6354E+02	2.5898E+04
14	2.3457E+00	2.2578E+03	2.8155E+04
15	2.2313E+00	5.6544E+03	3.3810E+04
16	1.9205E+00	5.5275E+03	3.9337E+04
17	1.6530E+00	7.2761E+03	4.6613E+04
18	1.3534E+00	9.5865E+03	5.6200E+04
19	1.0026E+00	5.9227E+03	6.2123E+04
20	8.2085E-01	3.4036E+03	6.5526E+04
21	7.4274E-01	6.3623E+03	7.1889E+04
22	6.0810E-01	5.7908E+03	7.7679E+04
23	4.9787E-01	6.7629E+03	8.4442E+04
24	3.6883E-01	5.0258E+03	8.9468E+04
25	2.9721E-01	9.4983E+03	9.8966E+04
26	1.8316E-01	7.8570E+03	1.0682E+05
27	1.1109E-01	6.7356E+03	1.1356E+05
28	6.7379E-02	5.9172E+03	1.1948E+05
29	4.0868E-02	2.7733E+03	1.2225E+05
	3.1828E-02		



TAB. A8

PCA-Replica - Calculated Neutron Spectrum in Mild Steel, in the 1/4 T RPV Measure Position No. 8 at Z = 39.01 cm.

Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGJEFF311.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	3.3794E+00	3.3794E+00
2	1.4191E+01	1.1280E+01	1.4659E+01
3	1.2214E+01	5.1558E+01	6.6217E+01
4	1.0000E+01	1.0107E+02	1.6729E+02
5	8.6071E+00	1.8408E+02	3.5137E+02
6	7.4082E+00	4.6030E+02	8.1167E+02
7	6.0653E+00	7.1022E+02	1.5219E+03
8	4.9659E+00	1.5958E+03	3.1177E+03
9	3.6788E+00	1.3268E+03	4.444E+03
10	3.0119E+00	9.7842E+02	5.4228E+03
11	2.7253E+00	1.1124E+03	6.5353E+03
12	2.4660E+00	5.7527E+02	7.1106E+03
13	2.3653E+00	1.5163E+02	7.2622E+03
14	2.3457E+00	8.0921E+02	8.0714E+03
15	2.2313E+00	2.2370E+03	1.0308E+04
16	1.9205E+00	2.6667E+03	1.2975E+04
17	1.6530E+00	3.8827E+03	1.6858E+04
18	1.3534E+00	6.5473E+03	2.3405E+04
19	1.0026E+00	4.9520E+03	2.8357E+04
20	8.2085E-01	2.3086E+03	3.0666E+04
21	7.4274E-01	7.8788E+03	3.8545E+04
22	6.0810E-01	5.9795E+03	4.4524E+04
23	4.9787E-01	7.8603E+03	5.2384E+04
24	3.6883E-01	7.1961E+03	5.9580E+04
25	2.9721E-01	8.2722E+03	6.7853E+04
26	1.8316E-01	7.7214E+03	7.5574E+04
27	1.1109E-01	4.6767E+03	8.0251E+04
28	6.7379E-02	3.2503E+03	8.3501E+04
29	4.0868E-02	9.4035E+02	8.4441E+04
	3.1828E-02		



TAB. A9

PCA-Replica - Calculated Neutron Spectrum in Mild Steel, in the 1/2 T RPV Position at Z = 44.21 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGJEFF311.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1 2 3 4 5 6	1.7332E+01 1.4191E+01 1.2214E+01 1.0000E+01 8.6071E+00 7.4082E+00	1.5429E+00 4.9718E+00 2.2247E+01 4.2528E+01 7.4699E+01 1.7704E+02	1.5429E+00 6.5147E+00 2.8762E+01 7.1290E+01 1.4599E+02 3.2303E+02
7	6.0653E+00	2.6357E+02	5.8660E+02
8	4.9659E+00	5.9457E+02	1.1812E+03
9	3.6788E+00	5.2654E+02	1.7077E+03
10	3.0119E+00	3.9107E+02	2.0988E+03
11	2.7253E+00	4.4417E+02	2.5429E+03
12	2.4660E+00	2.3066E+02	2.7736E+03
13	2.3653E+00	6.3351E+01	2.8369E+03
14	2.3457E+00	3.4587E+02	3.1828E+03
15	2.2313E+00	9.8509E+02	4.1679E+03
16	1.9205E+00	1.2810E+03	5.4489E+03
17	1.6530E+00	1.9557E+03	7.4046E+03
18	1.3534E+00	3.7030E+03	1.1108E+04
19	1.0026E+00	3.1840E+03	1.4292E+04
20	8.2085E-01	1.4368E+03	1.5728E+04
21	7.4274E-01	5.7268E+03	2.1455E+04
22	6.0810E-01	4.3925E+03	2.5848E+04
23	4.9787E-01	6.0140E+03	3.1862E+04
24	3.6883E-01	5.9460E+03	3.7808E+04
25	2.9721E-01	6.2975E+03	4.4105E+04
26	1.8316E-01	6.1859E+03	5.0291E+04
27	1.1109E-01	3.5556E+03	5.3847E+04
28	6.7379E-02	2.2957E+03	5.6142E+04
29	4.0868E-02 3.1828E-02	6.3091E+02	5.6773E+04



TAB. A10

PCA-Replica - Calculated Neutron Spectrum in Mild Steel, in the 3/4 T RPV Measure Position No. 9 at Z = 49.61 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGJEFF311.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	6.2648E-01	6.2648E-01
2	1.4191E+01	1.9511E+00	2.5775E+00
3	1.2214E+01	8.5431E+00	1.1121E+01
4	1.0000E+01	1.5937E+01	2.7057E+01
5	8.6071E+00	2.7075E+01	5.4132E+01
6	7.4082E+00	6.1179E+01	1.1531E+02
7	6.0653E+00	8.8944E+01	2.0426E+02
8	4.9659E+00	2.0425E+02	4.0851E+02
9	3.6788E+00	1.9293E+02	6.0144E+02
10	3.0119E+00	1.4317E+02	7.4461E+02
11	2.7253E+00	1.6309E+02	9.0771E+02
12	2.4660E+00	8.4772E+01	9.9248E+02
13	2.3653E+00	2.3936E+01	1.0164E+03
14	2.3457E+00	1.3439E+02	1.1508E+03
15	2.2313E+00	3.9450E+02	1.5453E+03
16	1.9205E+00	5.5341E+02	2.0987E+03
17	1.6530E+00	8.8019E+02	2.9789E+03
18	1.3534E+00	1.8471E+03	4.8260E+03
19	1.0026E+00	1.7997E+03	6.6257E+03
20	8.2085E-01	7.8435E+02	7.4100E+03
21	7.4274E-01	3.5607E+03	1.0971E+04
22	6.0810E-01	2.7471E+03	1.3718E+04
23	4.9787E-01	3.8052E+03	1.7523E+04
24	3.6883E-01	4.0621E+03	2.1585E+04
25	2.9721E-01	4.0690E+03	2.5654E+04
26	1.8316E-01	4.1648E+03	2.9819E+04
27	1.1109E-01	2.3002E+03	3.2119E+04
28	6.7379E-02	1.3961E+03	3.3515E+04
29	4.0868E-02 3.1828E-02	3.7714E+02	3.3892E+04



TAB. A11

PCA-Replica - Calculated Neutron Spectrum in Air, in the Void Box Measure Position No. 10 at Z = 58.61 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGJEFF311.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	2.0499E-01	2.0499E-01
2	1.4191E+01	6.2176E-01	8.2675E-01
3	1.2214E+01	2.6537E+00	3.4805E+00
4	1.0000E+01	4.8170E+00	8.2975E+00
5	8.6071E+00	7.9066E+00	1.6204E+01
6	7.4082E+00	1.6888E+01	3.3092E+01
7	6.0653E+00	2.3532E+01	5.6624E+01
8	4.9659E+00	5.2700E+01	1.0932E+02
9	3.6788E+00	4.9941E+01	1.5927E+02
10	3.0119E+00	3.6252E+01	1.9552E+02
11	2.7253E+00	4.0356E+01	2.3587E+02
12	2.4660E+00	2.1239E+01	2.5711E+02
13	2.3653E+00	6.2971E+00	2.6341E+02
14	2.3457E+00	3.5466E+01	2.9888E+02
15	2.2313E+00	1.0093E+02	3.9981E+02
16	1.9205E+00	1.4888E+02	5.4869E+02
17	1.6530E+00	2.3870E+02	7.8739E+02
18	1.3534E+00	5.3224E+02	1.3196E+03
19	1.0026E+00	5.8278E+02	1.9024E+03
20	8.2085E-01	2.2739E+02	2.1298E+03
21	7.4274E-01	1.1666E+03	3.2964E+03
22	6.0810E-01	8.6474E+02	4.1612E+03
23	4.9787E-01	1.0721E+03	5.2332E+03
24	3.6883E-01	1.3338E+03	6.5670E+03
25	2.9721E-01	1.2707E+03	7.8378E+03
26	1.8316E-01	1.2810E+03	9.1188E+03
27	1.1109E-01	6.5251E+02	9.7713E+03
28	6.7379E-02	3.4450E+02	1.0116E+04
29	4.0868E-02	7.5349E+01	1.0191E+04
	3.1828E-02		



di

APPENDIX B

Neutron Spectra Calculated along the Horizontal Axis Z Using BUGENDF70.BOLIB



TAB. B1

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 1 Measure Position No. 1 at Z = 1.91 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGENDF70.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.1762E+03	1.1762E+03
2	1.4191E+01	4.7219E+03	5.8982E+03
3	1.2214E+01	2.7127E+04	3.3025E+04
4	1.0000E+01	5.9888E+04	9.2913E+04
5	8.6071E+00	1.3371E+05	2.2662E+05
6	7.4082E+00	3.7646E+05	6.0308E+05
7	6.0653E+00	7.5508E+05	1.3582E+06
8	4.9659E+00	2.1623E+06	3.5205E+06
9	3.6788E+00	2.0551E+06	5.5756E+06
10	3.0119E+00	1.2818E+06	6.8573E+06
11	2.7253E+00	1.4504E+06	8.3077E+06
12	2.4660E+00	7.9502E+05	9.1027E+06
13	2.3653E+00	1.3826E+05	9.2410E+06
14	2.3457E+00	8.0829E+05	1.0049E+07
15	2.2313E+00	2.5504E+06	1.2600E+07
16	1.9205E+00	2.6829E+06	1.5283E+07
17	1.6530E+00	3.7006E+06	1.8983E+07
18	1.3534E+00	5.8049E+06	2.4788E+07
19	1.0026E+00	3.0613E+06	2.7849E+07
20	8.2085E-01	1.7244E+06	2.9574E+07
21	7.4274E-01	3.1775E+06	3.2751E+07
22	6.0810E-01	2.9351E+06	3.5686E+07
23	4.9787E-01	3.8772E+06	3.9564E+07
24	3.6883E-01	2.3256E+06	4.1889E+07
25	2.9721E-01	4.5967E+06	4.6486E+07
26	1.8316E-01	3.1859E+06	4.9672E+07
27	1.1109E-01	2.8708E+06	5.2543E+07
28	6.7379E-02	2.1944E+06	5.4737E+07
29	4.0868E-02	6.5589E+05	5.5393E+07
	3.1828E-02		



TAB. B2

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 1 Measure Position No. 2 at Z = 7.41 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGENDF70.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	3.2331E+02	3.2331E+02
2	1.4191E+01	1.2460E+03	1.5694E+03
3	1.2214E+01	6.7305E+03	8.2998E+03
4	1.0000E+01	1.4548E+04	2.2847E+04
5	8.6071E+00	3.1574E+04	5.4421E+04
6	7.4082E+00	9.1521E+04	1.4594E+05
7	6.0653E+00	1.7579E+05	3.2173E+05
8	4.9659E+00	4.7286E+05	7.9459E+05
9	3.6788E+00	4.0704E+05	1.2016E+06
10	3.0119E+00	2.7362E+05	1.4753E+06
11	2.7253E+00	3.2164E+05	1.7969E+06
12	2.4660E+00	1.6208E+05	1.9590E+06
13	2.3653E+00	3.3232E+04	1.9922E+06
14	2.3457E+00	1.8070E+05	2.1729E+06
15	2.2313E+00	4.9951E+05	2.6724E+06
16	1.9205E+00	4.8878E+05	3.1612E+06
17	1.6530E+00	6.5712E+05	3.8183E+06
18	1.3534E+00	8.9464E+05	4.7130E+06
19	1.0026E+00	5.4510E+05	5.2580E+06
20	8.2085E-01	3.2020E+05	5.5783E+06
21	7.4274E-01	5.5599E+05	6.1342E+06
22	6.0810E-01	5.1863E+05	6.6529E+06
23	4.9787E-01	6.0807E+05	7.2609E+06
24	3.6883E-01	4.4416E+05	7.7051E+06
25	2.9721E-01	8.6493E+05	8.5700E+06
26	1.8316E-01	7.1480E+05	9.2848E+06
27	1.1109E-01	6.1966E+05	9.9045E+06
28	6.7379E-02	5.4757E+05	1.0452E+07
29	4.0868E-02	2.5800E+05	1.0710E+07
	3.1828E-02		



TAB. B3

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 1 Measure Position No. 3 at Z = 12.41 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGENDF70.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.7691E+02	1.7691E+02
2	1.4191E+01	6.6200E+02	8.3891E+02
3	1.2214E+01	3.4228E+03	4.2618E+03
4	1.0000E+01	7.2430E+03	1.1505E+04
5	8.6071E+00	1.5124E+04	2.6628E+04
6	7.4082E+00	4.3264E+04	6.9892E+04
7	6.0653E+00	7.7401E+04	1.4729E+05
8	4.9659E+00	1.9168E+05	3.3897E+05
9	3.6788E+00	1.5276E+05	4.9173E+05
10	3.0119E+00	1.0624E+05	5.9797E+05
11	2.7253E+00	1.2427E+05	7.2224E+05
12	2.4660E+00	6.3314E+04	7.8556E+05
13	2.3653E+00	1.3801E+04	7.9936E+05
14	2.3457E+00	7.2304E+04	8.7166E+05
15	2.2313E+00	1.8894E+05	1.0606E+06
16	1.9205E+00	1.8037E+05	1.2410E+06
17	1.6530E+00	2.3896E+05	1.4799E+06
18	1.3534E+00	3.1554E+05	1.7955E+06
19	1.0026E+00	1.9264E+05	1.9881E+06
20	8.2085E-01	1.1158E+05	2.0997E+06
21	7.4274E-01	1.9764E+05	2.2973E+06
22	6.0810E-01	1.8272E+05	2.4800E+06
23	4.9787E-01	2.0969E+05	2.6897E+06
24	3.6883E-01	1.5339E+05	2.8431E+06
25	2.9721E-01	2.9382E+05	3.1369E+06
26	1.8316E-01	2.4128E+05	3.3782E+06
27	1.1109E-01	2.0949E+05	3.5877E+06
28	6.7379E-02	1.8405E+05	3.7718E+06
29	4.0868E-02	8.7474E+04	3.8592E+06
	3.1828E-02		



TAB. B4

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 1 Measure Position No. 4 at Z = 14.01 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGENDF70.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.4903E+02	1.4903E+02
2	1.4191E+01	5.5386E+02	7.0290E+02
3	1.2214E+01	2.8295E+03	3.5324E+03
4	1.0000E+01	5.9543E+03	9.4867E+03
5	8.6071E+00	1.2345E+04	2.1831E+04
6	7.4082E+00	3.5440E+04	5.7272E+04
7	6.0653E+00	6.2984E+04	1.2026E+05
8	4.9659E+00	1.5509E+05	2.7534E+05
9	3.6788E+00	1.2385E+05	3.9919E+05
10	3.0119E+00	8.7963E+04	4.8715E+05
11	2.7253E+00	1.0327E+05	5.9043E+05
12	2.4660E+00	5.3457E+04	6.4388E+05
13	2.3653E+00	1.1715E+04	6.5560E+05
14	2.3457E+00	6.2113E+04	7.1771E+05
15	2.2313E+00	1.6618E+05	8.8390E+05
16	1.9205E+00	1.6072E+05	1.0446E+06
17	1.6530E+00	2.1831E+05	1.2629E+06
18	1.3534E+00	3.0882E+05	1.5717E+06
19	1.0026E+00	1.8265E+05	1.7544E+06
20	8.2085E-01	1.0059E+05	1.8550E+06
21	7.4274E-01	2.0596E+05	2.0609E+06
22	6.0810E-01	1.8325E+05	2.2442E+06
23	4.9787E-01	2.0820E+05	2.4524E+06
24	3.6883E-01	1.5582E+05	2.6082E+06
25	2.9721E-01	2.6663E+05	2.8748E+06
26	1.8316E-01	2.3061E+05	3.1055E+06
27	1.1109E-01	1.8043E+05	3.2859E+06
28	6.7379E-02	1.6659E+05	3.4525E+06
29	4.0868E-02	6.9736E+04	3.5222E+06
	3.1828E-02		



TAB. B5

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 2 Measure Position No. 5 at Z = 19.91 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGENDF70.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	3.9701E+01	3.9701E+01
2	1.4191E+01	1.4480E+02	1.8450E+02
3	1.2214E+01	7.3693E+02	9.2143E+02
4	1.0000E+01	1.5551E+03	2.4766E+03
5	8.6071E+00	3.1735E+03	5.6500E+03
6	7.4082E+00	8.7594E+03	1.4409E+04
7	6.0653E+00	1.5664E+04	3.0073E+04
8	4.9659E+00	3.9485E+04	6.9558E+04
9	3.6788E+00	3.3256E+04	1.0281E+05
10	3.0119E+00	2.4216E+04	1.2703E+05
11	2.7253E+00	2.9308E+04	1.5634E+05
12	2.4660E+00	1.4877E+04	1.7121E+05
13	2.3653E+00	3.7387E+03	1.7495E+05
14	2.3457E+00	1.8774E+04	1.9373E+05
15	2.2313E+00	5.2465E+04	2.4619E+05
16	1.9205E+00	5.6421E+04	3.0261E+05
17	1.6530E+00	8.3437E+04	3.8605E+05
18	1.3534E+00	1.4141E+05	5.2746E+05
19	1.0026E+00	9.5436E+04	6.2290E+05
20	8.2085E-01	4.6055E+04	6.6895E+05
21	7.4274E-01	1.1326E+05	7.8222E+05
22	6.0810E-01	9.9227E+04	8.8144E+05
23	4.9787E-01	1.0152E+05	9.8296E+05
24	3.6883E-01	9.2465E+04	1.0754E+06
25	2.9721E-01	1.3132E+05	1.2067E+06
26	1.8316E-01	1.1283E+05	1.3196E+06
27	1.1109E-01	7.8889E+04	1.3985E+06
28	6.7379E-02	7.2550E+04	1.4710E+06
29	4.0868E-02	2.6943E+04	1.4980E+06
	3.1828E-02		
			1



TAB. B6

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 2 Measure Position No. 6 at Z = 25.41 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGENDF70.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.8840E+01	1.8840E+01
2	1.4191E+01	6.7162E+01	8.6002E+01
3	1.2214E+01	3.2797E+02	4.1398E+02
4	1.0000E+01	6.7406E+02	1.0880E+03
5	8.6071E+00	1.3321E+03	2.4202E+03
6	7.4082E+00	3.6344E+03	6.0545E+03
7	6.0653E+00	6.1469E+03	1.2201E+04
8	4.9659E+00	1.4273E+04	2.6474E+04
9	3.6788E+00	1.0925E+04	3.7399E+04
10	3.0119E+00	7.6602E+03	4.5060E+04
11	2.7253E+00	8.9811E+03	5.4041E+04
12	2.4660E+00	4.5397E+03	5.8581E+04
13	2.3653E+00	1.1434E+03	5.9724E+04
14	2.3457E+00	5.5358E+03	6.5260E+04
15	2.2313E+00	1.4139E+04	7.9399E+04
16	1.9205E+00	1.4045E+04	9.3444E+04
17	1.6530E+00	1.9054E+04	1.1250E+05
18	1.3534E+00	2.6075E+04	1.3857E+05
19	1.0026E+00	1.6530E+04	1.5510E+05
20	8.2085E-01	9.4839E+03	1.6459E+05
21	7.4274E-01	1.7356E+04	1.8194E+05
22	6.0810E-01	1.6251E+04	1.9819E+05
23	4.9787E-01	1.8564E+04	2.1676E+05
24	3.6883E-01	1.3674E+04	2.3043E+05
25	2.9721E-01	2.6455E+04	2.5689E+05
26	1.8316E-01	2.1824E+04	2.7871E+05
27	1.1109E-01	1.8879E+04	2.9759E+05
28	6.7379E-02	1.6663E+04	3.1425E+05
29	4.0868E-02	7.8494E+03	3.2210E+05
	3.1828E-02		



TAB. B7

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 2 Measure Position No. 7 at Z = 30.41 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGENDF70.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.0641E+01	1.0641E+01
2	1.4191E+01	3.6681E+01	4.7321E+01
3	1.2214E+01	1.7028E+02	2.1760E+02
4	1.0000E+01	3.4048E+02	5.5808E+02
5	8.6071E+00	6.5170E+02	1.2098E+03
6	7.4082E+00	1.7632E+03	2.9730E+03
7	6.0653E+00	2.8627E+03	5.8358E+03
8	4.9659E+00	6.3095E+03	1.2145E+04
9	3.6788E+00	4.5981E+03	1.6743E+04
10	3.0119E+00	3.1922E+03	1.9936E+04
11	2.7253E+00	3.7028E+03	2.3638E+04
12	2.4660E+00	1.8846E+03	2.5523E+04
13	2.3653E+00	4.7389E+02	2.5997E+04
14	2.3457E+00	2.2800E+03	2.8277E+04
15	2.2313E+00	5.6948E+03	3.3972E+04
16	1.9205E+00	5.5082E+03	3.9480E+04
17	1.6530E+00	7.2706E+03	4.6750E+04
18	1.3534E+00	9.6025E+03	5.6353E+04
19	1.0026E+00	5.9431E+03	6.2296E+04
20	8.2085E-01	3.4077E+03	6.5704E+04
21	7.4274E-01	6.3937E+03	7.2097E+04
22	6.0810E-01	5.8202E+03	7.7918E+04
23	4.9787E-01	6.7443E+03	8.4662E+04
24	3.6883E-01	5.0218E+03	8.9684E+04
25	2.9721E-01	9.4306E+03	9.9114E+04
26	1.8316E-01	7.8144E+03	1.0693E+05
27	1.1109E-01	6.7193E+03	1.1365E+05
28	6.7379E-02	5.9044E+03	1.1955E+05
29	4.0868E-02	2.7632E+03	1.2232E+05
	3.1028E-02		



TAB. B8

PCA-Replica - Calculated Neutron Spectrum in Mild Steel, in the 1/4 T RPV Measure Position No. 8 at Z = 39.01 cm.

Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGENDF70.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	3.3949E+00	3.3949E+00
2	1.4191E+01	1.1319E+01	1.4714E+01
3	1.2214E+01	5.1496E+01	6.6210E+01
4	1.0000E+01	1.0176E+02	1.6797E+02
5	8.6071E+00	1.8604E+02	3.5400E+02
6	7.4082E+00	4.7835E+02	8.3236E+02
7	6.0653E+00	7.3986E+02	1.5722E+03
8	4.9659E+00	1.5781E+03	3.1503E+03
9	3.6788E+00	1.2059E+03	4.3562E+03
10	3.0119E+00	9.4444E+02	5.3006E+03
11	2.7253E+00	1.1520E+03	6.4526E+03
12	2.4660E+00	6.0206E+02	7.0546E+03
13	2.3653E+00	1.6400E+02	7.2186E+03
14	2.3457E+00	8.1976E+02	8.0384E+03
15	2.2313E+00	2.2400E+03	1.0278E+04
16	1.9205E+00	2.5762E+03	1.2855E+04
17	1.6530E+00	3.7886E+03	1.6643E+04
18	1.3534E+00	6.7998E+03	2.3443E+04
19	1.0026E+00	4.7480E+03	2.8191E+04
20	8.2085E-01	2.2050E+03	3.0396E+04
21	7.4274E-01	8.2834E+03	3.8680E+04
22	6.0810E-01	5.8764E+03	4.4556E+04
23	4.9787E-01	7.4366E+03	5.1993E+04
24	3.6883E-01	7.3870E+03	5.9380E+04
25	2.9721E-01	7.8234E+03	6.7203E+04
26	1.8316E-01	7.4717E+03	7.4675E+04
27	1.1109E-01	4.7621E+03	7.9437E+04
28	6.7379E-02	3.3777E+03	8.2815E+04
29	4.0868E-02	9.2396E+02	8.3739E+04
	3.1828E-02		



TAB. B9

PCA-Replica - Calculated Neutron Spectrum in Mild Steel, in the 1/2 T RPV Position at Z = 44.21 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGENDF70.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.5378E+00	1.5378E+00
2	1.4191E+01	4.9714E+00	6.5092E+00
3	1.2214E+01	2.2147E+01	2.8656E+01
4	1.0000E+01	4.2975E+01	7.1631E+01
5	8.6071E+00	7.5635E+01	1.4727E+02
6	7.4082E+00	1.8461E+02	3.3187E+02
7	6.0653E+00	2.7841E+02	6.1028E+02
8	4.9659E+00	5.8593E+02	1.1962E+03
9	3.6788E+00	4.6270E+02	1.6589E+03
10	3.0119E+00	3.7177E+02	2.0307E+03
11	2.7253E+00	4.6054E+02	2.4912E+03
12	2.4660E+00	2.4350E+02	2.7347E+03
13	2.3653E+00	7.0339E+01	2.8051E+03
14	2.3457E+00	3.5248E+02	3.1575E+03
15	2.2313E+00	9.8359E+02	4.1411E+03
16	1.9205E+00	1.2316E+03	5.3727E+03
17	1.6530E+00	1.9046E+03	7.2773E+03
18	1.3534E+00	3.8928E+03	1.1170E+04
19	1.0026E+00	3.0178E+03	1.4188E+04
20	8.2085E-01	1.3454E+03	1.5533E+04
21	7.4274E-01	6.0376E+03	2.1571E+04
22	6.0810E-01	4.3214E+03	2.5892E+04
23	4.9787E-01	5.6354E+03	3.1528E+04
24	3.6883E-01	6.1327E+03	3.7660E+04
25	2.9721E-01	5.9129E+03	4.3573E+04
26	1.8316E-01	5.9303E+03	4.9503E+04
27	1.1109E-01	3.6182E+03	5.3122E+04
28	6.7379E-02	2.3999E+03	5.5522E+04
29	4.0868E-02	6.2230E+02	5.6144E+04
	3.1828E-02		



TAB. B10

PCA-Replica - Calculated Neutron Spectrum in Mild Steel, in the 3/4 T RPV Measure Position No. 9 at Z = 49.61 cm.

Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGENDF70.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	6.1917E-01	6.1917E-01
2	1.4191E+01	1.9438E+00	2.5630E+00
3	1.2214E+01	8.4864E+00	1.1049E+01
4	1.0000E+01	1.6185E+01	2.7234E+01
5	8.6071E+00	2.7510E+01	5.4744E+01
6	7.4082E+00	6.4161E+01	1.1890E+02
7	6.0653E+00	9.5374E+01	2.1428E+02
8	4.9659E+00	2.0082E+02	4.1510E+02
9	3.6788E+00	1.6446E+02	5.7956E+02
10	3.0119E+00	1.3399E+02	7.1355E+02
11	2.7253E+00	1.6862E+02	8.8218E+02
12	2.4660E+00	8.9874E+01	9.7205E+02
13	2.3653E+00	2.7148E+01	9.9920E+02
14	2.3457E+00	1.3767E+02	1.1369E+03
15	2.2313E+00	3.9261E+02	1.5295E+03
16	1.9205E+00	5.3023E+02	2.0597E+03
17	1.6530E+00	8.5779E+02	2.9175E+03
18	1.3534E+00	1.9685E+03	4.8860E+03
19	1.0026E+00	1.6909E+03	6.5768E+03
20	8.2085E-01	7.2203E+02	7.2989E+03
21	7.4274E-01	3.7599E+03	1.1059E+04
22	6.0810E-01	2.7242E+03	1.3783E+04
23	4.9787E-01	3.5415E+03	1.7324E+04
24	3.6883E-01	4.2083E+03	2.1533E+04
25	2.9721E-01	3.8158E+03	2.5348E+04
26	1.8316E-01	3.9639E+03	2.9312E+04
27	1.1109E-01	2.3347E+03	3.1647E+04
28	6.7379E-02	1.4582E+03	3.3105E+04
29	4.0868E-02	3.7188E+02	3.3477E+04
	3.1828E-02		



TAB. B11

PCA-Replica - Calculated Neutron Spectrum in Air, in the Void Box Measure Position No. 10 at Z = 58.61 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGENDF70.BOLIB/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	2.0002E-01	2.0002E-01
2	1.4191E+01	6.1084E-01	8.1086E-01
3	1.2214E+01	2.6299E+00	3.4408E+00
4	1.0000E+01	4.9359E+00	8.3767E+00
5	8.6071E+00	8.0956E+00	1.6472E+01
6	7.4082E+00	1.7836E+01	3.4309E+01
7	6.0653E+00	2.5574E+01	5.9883E+01
8	4.9659E+00	5.1672E+01	1.1155E+02
9	3.6788E+00	4.1714E+01	1.5327E+02
10	3.0119E+00	3.3636E+01	1.8690E+02
11	2.7253E+00	4.1174E+01	2.2808E+02
12	2.4660E+00	2.2489E+01	2.5057E+02
13	2.3653E+00	7.3108E+00	2.5788E+02
14	2.3457E+00	3.6675E+01	2.9455E+02
15	2.2313E+00	1.0081E+02	3.9536E+02
16	1.9205E+00	1.4399E+02	5.3935E+02
17	1.6530E+00	2.3771E+02	7.7706E+02
18	1.3534E+00	5.7977E+02	1.3568E+03
19	1.0026E+00	5.4872E+02	1.9056E+03
20	8.2085E-01	2.0482E+02	2.1104E+03
21	7.4274E-01	1.2289E+03	3.3392E+03
22	6.0810E-01	8.8933E+02	4.2286E+03
23	4.9787E-01	9.8103E+02	5.2096E+03
24	3.6883E-01	1.3889E+03	6.5985E+03
25	2.9721E-01	1.2108E+03	7.8093E+03
26	1.8316E-01	1.2104E+03	9.0198E+03
27	1.1109E-01	6.5962E+02	9.6794E+03
28	6.7379E-02	3.5452E+02	1.0034E+04
29	4.0868E-02	7.4601E+01	1.0109E+04
	3.1828E-02		


di

APPENDIX C

Neutron Spectra Calculated along the Horizontal Axis Z Using BUGLE-96



TAB. C1

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 1 Measure Position No. 1 at Z = 1.91 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGLE-96/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.1841E+03	1.1841E+03
2	1.4191E+01	4.7599E+03	5.9440E+03
3	1.2214E+01	2.7317E+04	3.3261E+04
4	1.0000E+01	6.0302E+04	9.3563E+04
5	8.6071E+00	1.3461E+05	2.2817E+05
6	7.4082E+00	3.7784E+05	6.0601E+05
7	6.0653E+00	7.6025E+05	1.3663E+06
8	4.9659E+00	2.1750E+06	3.5413E+06
9	3.6788E+00	2.0621E+06	5.6034E+06
10	3.0119E+00	1.2926E+06	6.8959E+06
11	2.7253E+00	1.4543E+06	8.3502E+06
12	2.4660E+00	7.9573E+05	9.1459E+06
13	2.3653E+00	1.3908E+05	9.2850E+06
14	2.3457E+00	8.1473E+05	1.0100E+07
15	2.2313E+00	2.5645E+06	1.2664E+07
16	1.9205E+00	2.7046E+06	1.5369E+07
17	1.6530E+00	3.7195E+06	1.9088E+07
18	1.3534E+00	5.8381E+06	2.4927E+07
19	1.0026E+00	3.0886E+06	2.8015E+07
20	8.2085E-01	1.7464E+06	2.9762E+07
21	7.4274E-01	3.2091E+06	3.2971E+07
22	6.0810E-01	2.9322E+06	3.5903E+07
23	4.9787E-01	3.9015E+06	3.9804E+07
24	3.6883E-01	2.3448E+06	4.2149E+07
25	2.9721E-01	4.6777E+06	4.6827E+07
26	1.8316E-01	3.2266E+06	5.0053E+07
27	1.1109E-01	2.7816E+06	5.2835E+07
28	6.7379E-02	2.1666E+06	5.5002E+07
29	4.0868E-02	6.4369E+05	5.5645E+07
	3.1828E-02		



TAB. C2

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 1 Measure Position No. 2 at Z = 7.41 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGLE-96/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	3.2771E+02	3.2771E+02
2	1.4191E+01	1.2563E+03	1.5840E+03
3	1.2214E+01	6.7761E+03	8.3601E+03
4	1.0000E+01	1.4593E+04	2.2953E+04
5	8.6071E+00	3.1456E+04	5.4409E+04
6	7.4082E+00	9.0473E+04	1.4488E+05
7	6.0653E+00	1.7661E+05	3.2149E+05
8	4.9659E+00	4.7070E+05	7.9219E+05
9	3.6788E+00	4.0698E+05	1.1992E+06
10	3.0119E+00	2.7519E+05	1.4744E+06
11	2.7253E+00	3.2038E+05	1.7947E+06
12	2.4660E+00	1.6028E+05	1.9550E+06
13	2.3653E+00	3.3274E+04	1.9883E+06
14	2.3457E+00	1.8028E+05	2.1686E+06
15	2.2313E+00	4.9602E+05	2.6646E+06
16	1.9205E+00	4.9022E+05	3.1548E+06
17	1.6530E+00	6.5757E+05	3.8124E+06
18	1.3534E+00	8.9436E+05	4.7067E+06
19	1.0026E+00	5.4409E+05	5.2508E+06
20	8.2085E-01	3.1992E+05	5.5708E+06
21	7.4274E-01	5.5670E+05	6.1275E+06
22	6.0810E-01	5.1915E+05	6.6466E+06
23	4.9787E-01	6.1006E+05	7.2567E+06
24	3.6883E-01	4.4573E+05	7.7024E+06
25	2.9721E-01	8.7212E+05	8.5745E+06
26	1.8316E-01	7.1963E+05	9.2942E+06
27	1.1109E-01	6.2207E+05	9.9162E+06
28	6.7379E-02	5.4950E+05	1.0466E+07
29	4.0868E-02	2.5902E+05	1.0725E+07
	3.1828E-02		



TAB. C3

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 1 Measure Position No. 3 at Z = 12.41 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGLE-96/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.7982E+02	1.7982E+02
2	1.4191E+01	6.6672E+02	8.4653E+02
3	1.2214E+01	3.4408E+03	4.2873E+03
4	1.0000E+01	7.2505E+03	1.1538E+04
5	8.6071E+00	1.4989E+04	2.6527E+04
6	7.4082E+00	4.2409E+04	6.8936E+04
7	6.0653E+00	7.7821E+04	1.4676E+05
8	4.9659E+00	1.9012E+05	3.3688E+05
9	3.6788E+00	1.5222E+05	4.8910E+05
10	3.0119E+00	1.0677E+05	5.9586E+05
11	2.7253E+00	1.2354E+05	7.1941E+05
12	2.4660E+00	6.2227E+04	7.8163E+05
13	2.3653E+00	1.3771E+04	7.9541E+05
14	2.3457E+00	7.1707E+04	8.6711E+05
15	2.2313E+00	1.8633E+05	1.0534E+06
16	1.9205E+00	1.7998E+05	1.2334E+06
17	1.6530E+00	2.3822E+05	1.4716E+06
18	1.3534E+00	3.1425E+05	1.7859E+06
19	1.0026E+00	1.9151E+05	1.9774E+06
20	8.2085E-01	1.1101E+05	2.0884E+06
21	7.4274E-01	1.9731E+05	2.2857E+06
22	6.0810E-01	1.8266E+05	2.4684E+06
23	4.9787E-01	2.0983E+05	2.6782E+06
24	3.6883E-01	1.5410E+05	2.8323E+06
25	2.9721E-01	2.9575E+05	3.1281E+06
26	1.8316E-01	2.4282E+05	3.3709E+06
27	1.1109E-01	2.1053E+05	3.5814E+06
28	6.7379E-02	1.8484E+05	3.7663E+06
29	4.0868E-02	8.7876E+04	3.8542E+06
	3.1828E-02		



TAB. C4

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 1 Measure Position No. 4 at Z = 14.01 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGLE-96/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.5163E+02	1.5163E+02
2	1.4191E+01	5.5778E+02	7.0941E+02
3	1.2214E+01	2.8435E+03	3.5529E+03
4	1.0000E+01	5.9565E+03	9.5094E+03
5	8.6071E+00	1.2221E+04	2.1731E+04
6	7.4082E+00	3.4697E+04	5.6428E+04
7	6.0653E+00	6.3426E+04	1.1985E+05
8	4.9659E+00	1.5400E+05	2.7386E+05
9	3.6788E+00	1.2326E+05	3.9712E+05
10	3.0119E+00	8.8485E+04	4.8560E+05
11	2.7253E+00	1.0286E+05	5.8847E+05
12	2.4660E+00	5.2601E+04	6.4107E+05
13	2.3653E+00	1.1680E+04	6.5275E+05
14	2.3457E+00	6.1583E+04	7.1433E+05
15	2.2313E+00	1.6400E+05	8.7834E+05
16	1.9205E+00	1.6016E+05	1.0385E+06
17	1.6530E+00	2.1770E+05	1.2562E+06
18	1.3534E+00	3.0766E+05	1.5638E+06
19	1.0026E+00	1.8186E+05	1.7457E+06
20	8.2085E-01	1.0021E+05	1.8459E+06
21	7.4274E-01	2.0517E+05	2.0511E+06
22	6.0810E-01	1.8415E+05	2.2352E+06
23	4.9787E-01	2.0751E+05	2.4427E+06
24	3.6883E-01	1.5916E+05	2.6019E+06
25	2.9721E-01	2.6554E+05	2.8674E+06
26	1.8316E-01	2.3797E+05	3.1054E+06
27	1.1109E-01	1.8096E+05	3.2864E+06
28	6.7379E-02	1.6644E+05	3.4528E+06
29	4.0868E-02	6.9884E+04	3.5227E+06
	3.1828E-02		



TAB. C5

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 2 Measure Position No. 5 at Z = 19.91 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGLE-96/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	4.0364E+01	4.0364E+01
2	1.4191E+01	1.4599E+02	1.8636E+02
3	1.2214E+01	7.4049E+02	9.2684E+02
4	1.0000E+01	1.5567E+03	2.4835E+03
5	8.6071E+00	3.1476E+03	5.6311E+03
6	7.4082E+00	8.5830E+03	1.4214E+04
7	6.0653E+00	1.5753E+04	2.9967E+04
8	4.9659E+00	3.9250E+04	6.9218E+04
9	3.6788E+00	3.3120E+04	1.0234E+05
10	3.0119E+00	2.4281E+04	1.2662E+05
11	2.7253E+00	2.9114E+04	1.5573E+05
12	2.4660E+00	1.4627E+04	1.7036E+05
13	2.3653E+00	3.6927E+03	1.7405E+05
14	2.3457E+00	1.8541E+04	1.9259E+05
15	2.2313E+00	5.1678E+04	2.4427E+05
16	1.9205E+00	5.5899E+04	3.0017E+05
17	1.6530E+00	8.2417E+04	3.8259E+05
18	1.3534E+00	1.3912E+05	5.2171E+05
19	1.0026E+00	9.3934E+04	6.1564E+05
20	8.2085E-01	4.5482E+04	6.6112E+05
21	7.4274E-01	1.0966E+05	7.7079E+05
22	6.0810E-01	9.9020E+04	8.6981E+05
23	4.9787E-01	9.7746E+04	9.6755E+05
24	3.6883E-01	9.1269E+04	1.0588E+06
25	2.9721E-01	1.2452E+05	1.1833E+06
26	1.8316E-01	1.1429E+05	1.2976E+06
27	1.1109E-01	7.8349E+04	1.3760E+06
28	6.7379E-02	7.3188E+04	1.4492E+06
29	4.0868E-02	2.6794E+04	1.4760E+06
	3.1828E-02		



TAB. C6

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 2 Measure Position No. 6 at Z = 25.41 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGLE-96/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.9259E+01	1.9259E+01
2	1.4191E+01	6.7753E+01	8.7012E+01
3	1.2214E+01	3.2960E+02	4.1661E+02
4	1.0000E+01	6.7299E+02	1.0896E+03
5	8.6071E+00	1.3112E+03	2.4008E+03
6	7.4082E+00	3.5219E+03	5.9227E+03
7	6.0653E+00	6.1636E+03	1.2086E+04
8	4.9659E+00	1.4070E+04	2.6156E+04
9	3.6788E+00	1.0830E+04	3.6986E+04
10	3.0119E+00	7.6631E+03	4.4649E+04
11	2.7253E+00	8.8785E+03	5.3528E+04
12	2.4660E+00	4.4267E+03	5.7954E+04
13	2.3653E+00	1.1284E+03	5.9083E+04
14	2.3457E+00	5.4360E+03	6.4519E+04
15	2.2313E+00	1.3805E+04	7.8324E+04
16	1.9205E+00	1.3863E+04	9.2186E+04
17	1.6530E+00	1.8754E+04	1.1094E+05
18	1.3534E+00	2.5592E+04	1.3653E+05
19	1.0026E+00	1.6190E+04	1.5272E+05
20	8.2085E-01	9.2963E+03	1.6202E+05
21	7.4274E-01	1.6992E+04	1.7901E+05
22	6.0810E-01	1.5985E+04	1.9499E+05
23	4.9787E-01	1.8248E+04	2.1324E+05
24	3.6883E-01	1.3460E+04	2.2670E+05
25	2.9721E-01	2.6102E+04	2.5280E+05
26	1.8316E-01	2.1490E+04	2.7429E+05
27	1.1109E-01	1.8536E+04	2.9283E+05
28	6.7379E-02	1.6371E+04	3.0920E+05
29	4.0868E-02	7.7129E+03	3.1691E+05
	3.1828E-02		



TAB. C7

PCA-Replica - Calculated Neutron Spectrum in Water, in the Water Gap 2 Measure Position No. 7 at Z = 30.41 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGLE-96/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.0921E+01	1.0921E+01
2	1.4191E+01	3.7001E+01	4.7922E+01
3	1.2214E+01	1.7103E+02	2.1895E+02
4	1.0000E+01	3.3920E+02	5.5816E+02
5	8.6071E+00	6.3794E+02	1.1961E+03
6	7.4082E+00	1.6962E+03	2.8923E+03
7	6.0653E+00	2.8699E+03	5.7622E+03
8	4.9659E+00	6.1988E+03	1.1961E+04
9	3.6788E+00	4.5410E+03	1.6502E+04
10	3.0119E+00	3.1879E+03	1.9690E+04
11	2.7253E+00	3.6535E+03	2.3343E+04
12	2.4660E+00	1.8309E+03	2.5174E+04
13	2.3653E+00	4.6689E+02	2.5641E+04
14	2.3457E+00	2.2305E+03	2.7872E+04
15	2.2313E+00	5.5367E+03	3.3408E+04
16	1.9205E+00	5.4171E+03	3.8825E+04
17	1.6530E+00	7.1381E+03	4.5964E+04
18	1.3534E+00	9.4077E+03	5.5371E+04
19	1.0026E+00	5.8127E+03	6.1184E+04
20	8.2085E-01	3.3348E+03	6.4519E+04
21	7.4274E-01	6.2562E+03	7.0775E+04
22	6.0810E-01	5.7215E+03	7.6496E+04
23	4.9787E-01	6.6156E+03	8.3112E+04
24	3.6883E-01	4.9529E+03	8.8065E+04
25	2.9721E-01	9.3278E+03	9.7393E+04
26	1.8316E-01	7.7162E+03	1.0511E+05
27	1.1109E-01	6.6186E+03	1.1173E+05
28	6.7379E-02	5.8182E+03	1.1755E+05
29	4.0868E-02	2.7223E+03	1.2027E+05
	3.1828E-02		



TAB. C8

PCA-Replica - Calculated Neutron Spectrum in Mild Steel, in the 1/4 T RPV Measure Position No. 8 at Z = 39.01 cm.

Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGLE-96/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	3.4737E+00	3.4737E+00
2	1.4191E+01	1.1399E+01	1.4872E+01
3	1.2214E+01	5.1584E+01	6.6456E+01
4	1.0000E+01	1.0141E+02	1.6787E+02
5	8.6071E+00	1.8290E+02	3.5076E+02
6	7.4082E+00	4.6178E+02	8.1254E+02
7	6.0653E+00	7.4479E+02	1.5573E+03
8	4.9659E+00	1.5645E+03	3.1219E+03
9	3.6788E+00	1.1902E+03	4.3121E+03
10	3.0119E+00	9.4144E+02	5.2536E+03
11	2.7253E+00	1.1400E+03	6.3936E+03
12	2.4660E+00	5.8800E+02	6.9816E+03
13	2.3653E+00	1.6066E+02	7.1422E+03
14	2.3457E+00	8.0201E+02	7.9442E+03
15	2.2313E+00	2.1889E+03	1.0133E+04
16	1.9205E+00	2.5260E+03	1.2659E+04
17	1.6530E+00	3.7139E+03	1.6373E+04
18	1.3534E+00	6.6477E+03	2.3021E+04
19	1.0026E+00	4.6547E+03	2.7675E+04
20	8.2085E-01	2.1730E+03	2.9848E+04
21	7.4274E-01	8.0621E+03	3.7911E+04
22	6.0810E-01	5.8941E+03	4.3805E+04
23	4.9787E-01	7.1857E+03	5.0990E+04
24	3.6883E-01	7.5062E+03	5.8497E+04
25	2.9721E-01	7.9090E+03	6.6406E+04
26	1.8316E-01	7.4943E+03	7.3900E+04
27	1.1109E-01	4.8164E+03	7.8716E+04
28	6.7379E-02	3.3931E+03	8.2109E+04
29	4.0868E-02	9.2254E+02	8.3032E+04
	3.1828E-02		



TAB. C9

PCA-Replica - Calculated Neutron Spectrum in Mild Steel, in the 1/2 T RPV Position at Z = 44.21 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGLE-96/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	1.5701E+00	1.5701E+00
2	1.4191E+01	5.0053E+00	6.5755E+00
3	1.2214E+01	2.2170E+01	2.8745E+01
4	1.0000E+01	4.2852E+01	7.1597E+01
5	8.6071E+00	7.4498E+01	1.4610E+02
6	7.4082E+00	1.7827E+02	3.2437E+02
7	6.0653E+00	2.8005E+02	6.0441E+02
8	4.9659E+00	5.8134E+02	1.1858E+03
9	3.6788E+00	4.5648E+02	1.6422E+03
10	3.0119E+00	3.7004E+02	2.0123E+03
11	2.7253E+00	4.5554E+02	2.4678E+03
12	2.4660E+00	2.3793E+02	2.7057E+03
13	2.3653E+00	6.8767E+01	2.7745E+03
14	2.3457E+00	3.4453E+02	3.1190E+03
15	2.2313E+00	9.6131E+02	4.0803E+03
16	1.9205E+00	1.2051E+03	5.2854E+03
17	1.6530E+00	1.8617E+03	7.1471E+03
18	1.3534E+00	3.7907E+03	1.0938E+04
19	1.0026E+00	2.9465E+03	1.3884E+04
20	8.2085E-01	1.3241E+03	1.5208E+04
21	7.4274E-01	5.8394E+03	2.1048E+04
22	6.0810E-01	4.3366E+03	2.5384E+04
23	4.9787E-01	5.4105E+03	3.0795E+04
24	3.6883E-01	6.2264E+03	3.7021E+04
25	2.9721E-01	6.0019E+03	4.3023E+04
26	1.8316E-01	5.9597E+03	4.8983E+04
27	1.1109E-01	3.6842E+03	5.2667E+04
28	6.7379E-02	2.4310E+03	5.5098E+04
29	4.0868E-02	6.2649E+02	5.5725E+04
	3.1828E-02		



TAB. C10

PCA-Replica - Calculated Neutron Spectrum in Mild Steel, in the 3/4 T RPV Measure Position No. 9 at Z = 49.61 cm.

Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGLE-96/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	6.3163E-01	6.3163E-01
2	1.4191E+01	1.9578E+00	2.5894E+00
3	1.2214E+01	8.4931E+00	1.1083E+01
4	1.0000E+01	1.6143E+01	2.7226E+01
5	8.6071E+00	2.7120E+01	5.4346E+01
6	7.4082E+00	6.1939E+01	1.1629E+02
7	6.0653E+00	9.5853E+01	2.1214E+02
8	4.9659E+00	1.9930E+02	4.1143E+02
9	3.6788E+00	1.6215E+02	5.7358E+02
10	3.0119E+00	1.3320E+02	7.0678E+02
11	2.7253E+00	1.6670E+02	8.7349E+02
12	2.4660E+00	8.7861E+01	9.6135E+02
13	2.3653E+00	2.6501E+01	9.8785E+02
14	2.3457E+00	1.3444E+02	1.1223E+03
15	2.2313E+00	3.8363E+02	1.5059E+03
16	1.9205E+00	5.1749E+02	2.0234E+03
17	1.6530E+00	8.3549E+02	2.8589E+03
18	1.3534E+00	1.9061E+03	4.7650E+03
19	1.0026E+00	1.6405E+03	6.4055E+03
20	8.2085E-01	7.0807E+02	7.1136E+03
21	7.4274E-01	3.5984E+03	1.0712E+04
22	6.0810E-01	2.7238E+03	1.3436E+04
23	4.9787E-01	3.3712E+03	1.6807E+04
24	3.6883E-01	4.2346E+03	2.1042E+04
25	2.9721E-01	3.8631E+03	2.4905E+04
26	1.8316E-01	3.9604E+03	2.8865E+04
27	1.1109E-01	2.3780E+03	3.1243E+04
28	6.7379E-02	1.4820E+03	3.2725E+04
29	4.0868E-02	3.7572E+02	3.3101E+04
	3.1828E-02		



TAB. C11

PCA-Replica - Calculated Neutron Spectrum in Air, in the Void Box Measure Position No. 10 at Z = 58.61 cm.

> Group Neutron Fluxes per Fission Plate Watt. [neutrons \times cm⁻² \times s⁻¹ \times Plate Watt⁻¹]

Group	Upper Energy [MeV]	BUGLE-96/ TORT-3.2 (X,Y,Z) Neutron Flux	Cumulative Neutron Flux
1	1.7332E+01	2.0412E-01	2.0412E-01
2	1.4191E+01	6.1562E-01	8.1974E-01
3	1.2214E+01	2.6325E+00	3.4522E+00
4	1.0000E+01	4.9234E+00	8.3756E+00
5	8.6071E+00	7.9830E+00	1.6359E+01
6	7.4082E+00	1.7205E+01	3.3564E+01
7	6.0653E+00	2.5670E+01	5.9234E+01
8	4.9659E+00	5.1293E+01	1.1053E+02
9	3.6788E+00	4.1125E+01	1.5165E+02
10	3.0119E+00	3.3395E+01	1.8505E+02
11	2.7253E+00	4.0627E+01	2.2567E+02
12	2.4660E+00	2.1930E+01	2.4760E+02
13	2.3653E+00	7.1157E+00	2.5472E+02
14	2.3457E+00	3.5718E+01	2.9044E+02
15	2.2313E+00	9.8204E+01	3.8864E+02
16	1.9205E+00	1.3977E+02	5.2841E+02
17	1.6530E+00	2.2966E+02	7.5806E+02
18	1.3534E+00	5.5408E+02	1.3121E+03
19	1.0026E+00	5.2541E+02	1.8376E+03
20	8.2085E-01	1.9882E+02	2.0364E+03
21	7.4274E-01	1.1484E+03	3.1848E+03
22	6.0810E-01	8.7607E+02	4.0609E+03
23	4.9787E-01	9.1092E+02	4.9718E+03
24	3.6883E-01	1.3530E+03	6.3248E+03
25	2.9721E-01	1.2000E+03	7.5248E+03
26	1.8316E-01	1.1840E+03	8.7088E+03
27	1.1109E-01	6.5810E+02	9.3669E+03
28	6.7379E-02	3.5778E+02	9.7247E+03
29	4.0868E-02	7.3424E+01	9.7981E+03
	3.1828E-02		